



Mestrado Integrado em  
Engenharia Electrotécnica e de Computadores

**Controlo Em Espaço de Estados**

2015/2016

**Second Test**

25 May 2016, 18h30 – rooms EA5, EA2

**Duration 2 hours**

**No consultation of any kind allowed nor programmable means**

**Grading:** P1-a)1 b)3 c)2, P2-a)1 b)3 c)1, P3-5, P4-a)3 b)1.

**P1.** The pendulum is described by equations that are the same for other systems of practical interest, such as an electrical power generator connected to a power transmission line. Consider the model of the pendulum that is described by the following nonlinear state equations:

$$\frac{dx_1}{dt} = x_2$$

$$\frac{dx_2}{dt} = 9 \sin(x_1)$$

- a) Show that the states  $\bar{x}^1 = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$  e  $\bar{x}^2 = \begin{bmatrix} \pi \\ 0 \end{bmatrix}$  are two equilibrium points.
- b) Get the equations of the linearized system around each of the equilibrium points.
- c) Based on the results obtained on b) what can you say about the stability of each of the equilibrium points of the **nonlinear system** referred on a)?



**P2.** In this problem you have two alternatives, named A and B. Alternative A is more complicated, but has an higher grading (5 points), whereas alternative B is evaluated only 2 points. **You must indicate which alternative you choose. If you answer to both alternatives only the answer to A is considered.**

**A)** In this problem the stability of a satellite actuated by a nonlinear controller is considered. For the sake of simplicity, it is assumed that the satellite moves only

in one plane. Let  $\theta$  be the satellite angle with respect to a reference direction,  $\omega$  the corresponding angular velocity, and  $u$  the torque (manipulated variable) that is applied to the satellite by jets. The state model is therefore

$$\begin{aligned}\frac{d\theta}{dt} &= \omega \\ \frac{d\omega}{dt} &= u\end{aligned}$$

The control law computes  $u$  as a function of the measures of  $\theta$  and  $\omega$ , and is given by

$$u = -g(\omega) - h(\theta),$$

Where the functions  $g$  and  $h$  (there are several possibilities) satisfy

$$g(0) = 0 \text{ and } \omega g(\omega) > 0 \text{ for } \omega \neq 0$$

$$h(0) = 0 \text{ and } \theta h(\theta) > 0 \text{ for } \theta \neq 0$$

- Show that, with this control law, the origin  $\theta = 0$  and  $\omega = 0$  (the satellite stopped and turned to the reference direction) is an equilibrium point.
- What can you say about the stability of this equilibrium point using the Lyapunov function  $(\theta, \omega) = \frac{1}{2}\omega^2 + \int_0^\theta h(\sigma)d\sigma$  ?
- At each time instant  $t$ , the manipulated variable  $u(t)$  must be within the boundary values:  $-u_{max} \leq u(t) \leq u_{max}$ . Give an example of functions  $g$  and  $h$  that ensure that the origin is asymptotically stable and that at the same time ensure this interval of values for  $u(t)$ .


**B)** Consider the system described by the nonlinear state equations

$$\begin{aligned}\frac{dx_1}{dt} &= -x_1 - x_1x_2^2 \\ \frac{dx_2}{dt} &= -x_2 - x_1^2x_2\end{aligned}$$

For this system, the origin ( $x_1 = 0, x_2 = 0$ ) is an equilibrium point. With respect to this equilibrium point, take as candidate Lyapunov function

$$V(x_1, x_2) = \frac{1}{2}(x_1^2 + x_2^2).$$

What can you say about the stability of this equilibrium point for the nonlinear system? Show all computations.



**P3.** Consider an electrical energy production plant that uses a thermal solar collector. The fluid to be heated by the sun circulates by the action of a pump and is used to produce electrical energy in a thermoelectric group. The model (very simplified) that relates the power produced  $x$  with the pump command  $u$  (in normalized units, with  $u = 0$  corresponding to the pump stop and  $u = 1$  corresponding to the maximum velocity) is given by the scalar differential equation


$$\frac{dx}{dt} = -0,2x + u$$

Starting from a situation in which no power is being produced (meaning that  $x(0) = 0$ ), we want to find the function  $u$  in the time interval between  $t = 0$  and  $t = 5$  that maximizes the functional

$$J(u) = \int_0^5 [x(t) - u(t)]dt, \quad 0 \leq u \leq 1.$$

This functional represents a compromise between producing the maximum of energy at the end of the optimization interval, on one side, and consuming less energy on the pump. By using Pontryagin's Principle **obtain the optimal control**.

Sketch qualitatively, but indicating the important points, the plots of the Hamiltonian, of the co-state, of the optimal control, and of the power produced in the time interval between  $t = 0$  e  $t = 5$ .



**P4.** Consider a vehicle that moves along a straight line, always in the same direction, and where the  $v$  is related with the rate of fuel consumption  $u$  by

$$\frac{dv}{dt} = -v + u.$$

Initially the velocity is zero,  $v(0) = 0$ . We want to control the vehicle in the time interval  $[0, T]$ , so that the final velocity has the value  $v(T) = V_2$ , and such as to minimize the fuel spent in the manoeuver

$$J(u) = \int_0^T u(t)dt.$$

The following constraint must be respected

$$0 \leq u(t) \leq u_{max}$$

Above,  $V_2$ ,  $T$  and  $u_{max}$  are parameters with well defined and assumed known values. The answer must be expressed in terms of them.

- Using Pontryagin's Principle, find the optimal control that solves this problem. Sketch qualitatively, but indicating the important points, the plots of the Hamiltonian, of the co-state, and of the optimal control.
- Discuss the existence of solution for the optimal control problem as a function of the parameters  $V_2$ ,  $T$  e  $u_{max}$ .



### Useful help

$$\dot{x} = -ax + b \quad a, b \text{ constants}$$

$$x(t) = \frac{b}{a} + C e^{-at}$$

$$\frac{dx}{dt} = f(x, u) \quad x(0) = x_0 \quad J(u) = \Psi(x(T)) + \int_0^T L(x, u) dt$$

$$-\left(\frac{d\lambda}{dt}\right)' = \lambda'(t) f_x(x(t), u(t)) + L_x(x(t), u(t)) \quad \lambda(T) = \Psi_x(x(T))$$

$$H(\lambda, x, u) = \lambda' f(x, u) + L(x, u)$$

$$f_x = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} \\ \frac{\partial f_2}{\partial x_1} & \frac{\partial f_2}{\partial x_2} \end{bmatrix} \quad L_x = \begin{bmatrix} \frac{\partial L}{\partial x_1} & \frac{\partial L}{\partial x_2} \end{bmatrix} \quad \Psi_x = \begin{bmatrix} \frac{\partial \Psi}{\partial x_1} & \frac{\partial \Psi}{\partial x_2} \end{bmatrix}$$