

3 a) eq. (6.9):  $L = \frac{\rho l}{A} = \frac{10^3 \times 50}{0,01} = 5 \times 10^6 \text{ (SI)}$

b)  $\underbrace{pg\bar{h}}_{\text{pressão no fundo do tanque}} = \bar{P}_r \Rightarrow \bar{h} = \frac{8 \times 10^4}{10^3 \times 9,8} = 8,16 \text{ m}$

c)  $Q_r = 0,3 \times 10^{-4} N \sqrt{P_r}$  condições nominais  $0,01 = 0,3 \times 10^{-4} \bar{N} \sqrt{8 \times 10^4} \Leftrightarrow$   
valor nominal de N  $\Leftrightarrow \bar{N} = \frac{0,01}{0,3 \times 10^{-4} \sqrt{8 \times 10^4}} = 1,18$

$Q_r - \bar{Q}_r = \frac{\partial Q_r}{\partial N} \Big|_{\bar{N}, \bar{P}_r} \times (N - \bar{N}) + \frac{\partial Q_r}{\partial P_r} \Big|_{\bar{N}, \bar{P}_r} \times (P_r - \bar{P}_r)$   
derivadas face aos valores nominais derivadas parciais nas condições nominais

$Q_r = 0,01 + 0,3 \times 10^{-4} \sqrt{8 \times 10^4} (N - 1,18) + 0,3 \times 10^{-4} \times 1,18 \times \frac{1}{2\sqrt{8 \times 10^4}} (P_r - 8 \times 10^4) =$   
 $= 0,01 + 8,5 \times 10^{-3} (N - 1,18) + 6,25 \times 10^{-8} (P_r - 8 \times 10^4)$

(pois  $\frac{\partial Q_r}{\partial N} = 0,3 \times 10^{-4} \sqrt{P_r}$  e  $\frac{\partial Q_r}{\partial P_r} = 0,3 \times 10^{-4} N \times \frac{1}{2} \times \frac{1}{\sqrt{P_r}}$ )

d)  $P_r = pg h$  logo, em condições nominais,  $\bar{P}_r = pg \bar{h}$  e subtraindo nas  
 $P_r - \bar{P}_r = pg (h - \bar{h})$  isto é 0 porque as condições nominais são constantes

$Q - Q_r = A \dot{h}$  logo, em condições nominais  $\bar{Q} - \bar{Q}_r = A \dot{\bar{h}}$  e subtraindo na  
conservação da massa, a.k.a. a água para algum lado tem de ir

$Q - \bar{Q} - Q_r + \bar{Q}_r = A(\dot{h} - \dot{\bar{h}}) = A \frac{d}{dt}(h - \bar{h})$

eq. (6.8) } ou então  
 eq. (6.9) } (6.12) + (6.1)  
 derivada }  $P - P_r = L \dot{Q}$  em condições nominais  $\bar{P} - \bar{P}_r = L \dot{\bar{Q}}$  e subtraindo

$P - \bar{P} - P_r + \bar{P}_r = L(\dot{Q} - \dot{\bar{Q}}) = L \frac{d}{dt}(Q - \bar{Q})$

e) Temos 4 equações; aplicando 1o mem

$$\begin{cases} \Delta P_{nr} = \rho g \Delta h \\ \Delta Q - \Delta Q_{nr} = A_s \Delta h \\ \Delta P - \Delta P_{nr} = L_s \Delta Q \\ \Delta Q_{nr} = \alpha \Delta N + \beta \Delta P_{nr} \end{cases} \begin{cases} \Delta h = \frac{1}{\rho g} \Delta P_{nr} \\ \Delta Q = \Delta Q_{nr} + \frac{A_s}{\rho g} \Delta P_{nr} \\ \Delta P = \Delta P_{nr} + L_s \Delta Q_{nr} + \frac{L A_s^2}{\rho g} \Delta P_{nr} = \Delta Q_{nr} \times L_s + \Delta P_{nr} \times \left(1 + \frac{L A_s^2}{\rho g}\right) \\ \Delta Q_{nr} = \alpha \Delta N + \beta \Delta P_{nr} \end{cases}$$

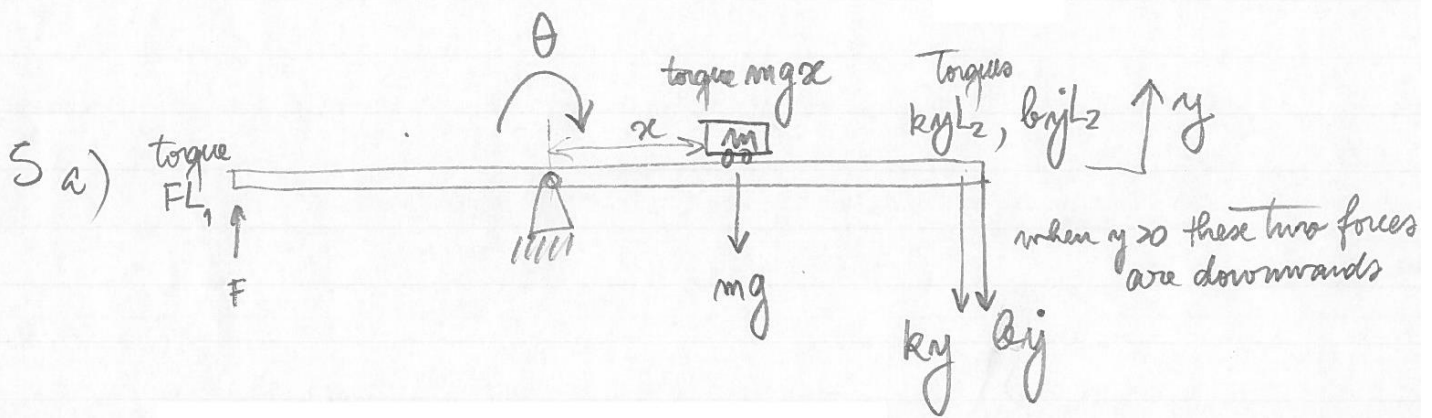
$8,5 \times 10^{-3}$        $6,25 \times 10^{-8}$

$$\Delta P = \alpha L_s \Delta N + \beta L_s \Delta P_{nr} + \Delta P_{nr} \left(1 + \frac{L A_s^2}{\rho g}\right) =$$

$$= \alpha L_s \Delta N + \left(1 + \beta L_s + \frac{L A_s^2}{\rho g}\right) \Delta P_{nr}$$

P/achar a F.T. fazemos  $\Delta P = 0$  e vem  $\frac{\Delta P_{nr}}{\Delta N} = \frac{-\alpha L_s}{\frac{L A_s^2}{\rho g} + \beta L_s + 1} =$

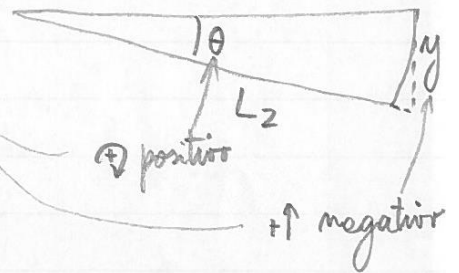
$$= \frac{-8,5 \times 10^{-3} \times 5 \times 10^6}{\frac{50 \times 0,01}{9,8 \times 10^3} + 6,25 \times 10^{-8} \times 5 \times 10^6 + 1}$$



$$I \ddot{\theta} = FL_1 + mgx + kyL_2 + byL_2$$

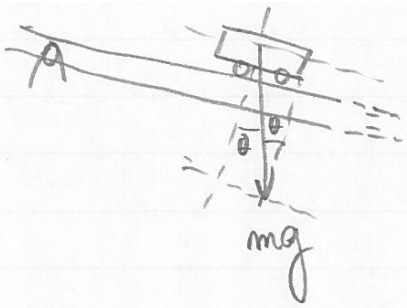
se  $\theta \approx 0$  então  $\sin \theta \approx \theta$  logo

$$\theta \approx \frac{-y}{L_2} \Leftrightarrow y = -\theta L_2$$



$$I \ddot{\theta} = FL_1 + mgx - k \theta L_2^2 - b \dot{\theta} L_2^2$$

equação 1



peso:  $mg$   
 componente perpendicular:  $mg \cos \theta \approx mg$   
 " tangencial:  $mg \sin \theta \approx mg \theta$   
 $m \ddot{x} = mg \theta \Leftrightarrow \ddot{x} = g \theta$  equação 2

$$b) \begin{cases} I \theta^2 \text{ (H)} = FL_1 + mg X - k L_2^2 \text{ (H)} - b L_2^2 \dot{\theta} \text{ (H)} \\ X \theta^2 = g \text{ (H)} \end{cases}$$

$$\begin{cases} (I \theta^2 + k L_2^2 + b L_2^2 \dot{\theta}) \frac{\theta^2}{g} X = FL_1 + mg X \\ \text{(H)} = \frac{\theta^2}{g} X \end{cases}$$

$$(I \theta^4 + b L_2^2 \dot{\theta}^3 + k L_2^2 \dot{\theta}^2) X - mg^2 X = FL_1 g$$

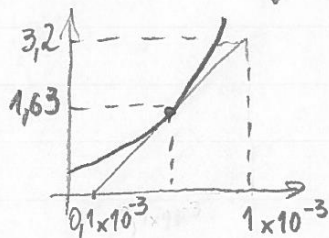
$$\frac{X}{F} = \frac{L_1 g}{I \theta^4 + b L_2^2 \dot{\theta}^3 + k L_2^2 \dot{\theta}^2 - mg^2}$$

6a) Em equilíbrio, o balanço de momentos é

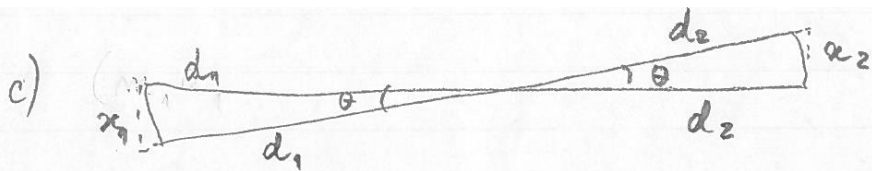
$$0 = \overline{F}_m d_1 + m_1 g d_1 - m_2 g d_2 \Rightarrow \overline{F}_m = \frac{9,8}{0,6} (2 \times 0,4 - 1,5 \times 0,6) = 1,63$$

$\begin{matrix} \text{200g} \\ \text{mola} \end{matrix}$

b) Por leitura no gráfico, o declive é  $\frac{3,2}{0,9 \times 10^{-3}} = 3,56 \times 10^3$



Logo  $F_m = \underbrace{1,63}_{\overline{F}_m} + 3,56 \times 10^3 x_1$



$$\theta \approx \sin \theta = \frac{\alpha_1}{d_1}$$

$$\alpha_1 = \theta d_1$$

$$\theta \approx \sin \theta = \frac{\alpha_2}{d_2}$$

$$\alpha_2 = \theta d_2$$

Balanco de momentos:  
momento de inercia J

$$(m_1 d_1^2 + m_2 d_2^2) \ddot{\theta} = T - F_m d_1 - F_b d_2 + m_1 g d_1 - m_2 g d_2$$

$$J \ddot{\theta} = T - \underbrace{(F_m d_1 + 3,56 \times 10^3 \alpha_1 d_1)}_{\substack{\uparrow \\ \text{estes termos caem (por alinhamento)}}} - \underbrace{b \alpha_2 d_2}_{\substack{\uparrow \\ \text{estes termos caem (por alinhamento)}}} + m_1 g d_1 - m_2 g d_2$$

$$J \ddot{\theta} = T - 3,56 \times 10^3 d_1^2 \theta - b d_2^2 \theta$$

substituindo

$$(1,5 \times 0,6^2 + 2 \times 0,4^2) \ddot{\theta} + 3,56 \times 10^3 \times 0,6^2 \theta + 20 \times 0,4^2 \theta = T$$

$$0,86 \ddot{\theta} + 3,2 \dot{\theta} + 1282 \theta = T$$

$$\Rightarrow (0,86 \text{ s}^2 + 3,2 \text{ s} + 1282) \ddot{\theta} = T \Rightarrow \frac{\ddot{\theta}}{T} = \frac{1}{0,86 \text{ s}^2 + 3,2 \text{ s} + 1282}$$

Balanco de forças:

o que sobra  
sobre  
nessa  
deriva

$$0 = F - m_1 g - m_2 g + F_m - F_b - \underbrace{m_1 \ddot{x}_1 + m_2 \ddot{x}_2}_{\substack{\text{"forças" resultantes do movimento}}}$$

$$F = \underbrace{m_1 g + m_2 g - 1,63}_{\text{constantes}} - 3,56 \times 10^3 \underbrace{\alpha_1}_{\theta d_1} + b \underbrace{\alpha_2}_{\theta d_2} + \underbrace{m_1 \ddot{x}_1}_{m_1 \ddot{\theta} d_1} - \underbrace{m_2 \ddot{x}_2}_{m_2 \ddot{\theta} d_2}$$

$$\Delta F = \underbrace{(2 \times 0,4 + 1,5 \times 0,6)}_{0,1} \ddot{\theta} + \underbrace{(20 \times 0,4)}_8 \dot{\theta} - \underbrace{3,56 \times 10^3 \times 0,6}_{2136} \theta$$

$$\frac{\Delta F}{\ddot{\theta}} = 0,1 \text{ s}^2 + 8 \text{ s} - 2136$$

$$\text{Logo } \frac{\Delta F}{T} = \frac{\Delta F}{(H)} \times \frac{(H)}{T} = \frac{0,1s^2 + 8s - 2136}{0,86s^2 + 3,2s + 1282}$$

7a) Em condições nominais,  $\bar{q}_c = \bar{q}_1 = 0,2$  logo

$$q_1 = 0,15 \alpha_n \sqrt{\Delta p} \Rightarrow 0,2 = 0,15 \alpha_n \sqrt{\rho g (R_0 - h_1)} = 0,15 \alpha_n \sqrt{9,8 \times 10^3 \times 2}$$

$$\Rightarrow \alpha_n = \frac{0,2}{0,15 \sqrt{9,8 \times 2 \times 10^3}} = 9,5 \times 10^{-3}$$

$$q_1 - \bar{q}_1 = \underbrace{\frac{\partial q_1}{\partial \alpha_n} \Big|_{\bar{\alpha}_n, \bar{\Delta p}}}_{0,15 \sqrt{\Delta p}} \times (\alpha_n - \bar{\alpha}_n) + \underbrace{\frac{\partial q_1}{\partial \Delta p} \Big|_{\bar{\alpha}_n, \bar{\Delta p}}}_{0,15 \bar{\alpha}_n \frac{1}{2} \frac{1}{\sqrt{\Delta p}}}$$

$$\underbrace{0,15 \sqrt{9,8 \times 10^3 \times 2}}_{21} \quad \underbrace{0,15 \times 9,5 \times 10^{-3} \times \frac{1}{2} \times \frac{1}{\sqrt{9,8 \times 10^3 \times 2}}}_{5,09 \times 10^{-6}}$$

$$\Delta q_1 = 21 \Delta \alpha_n + 5,09 \times 10^{-6} (\Delta p - 2)$$

$$q_1 - 0,2 \quad \alpha_n - 9,5 \times 10^{-3}$$