

**Reliability and Quality Control**

1st. Test (“RECURSO”)

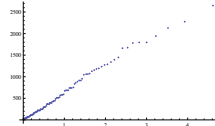
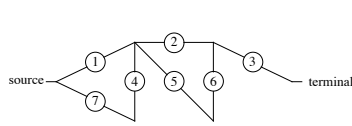
2nd. Semester — 2012/13

Duration: 1h30m

2013/06/28 — 6:30PM, Room P8

- Please justify your answers.
- This test has **one page** and **three questions**. The total of points is **20.0**.

1. A communication network is set as pictured below on the left and only operates if the source is connected to the terminal.



Communication network (left, question 1); exponential probability plot (right, question 3).

(a) Find the minimal path sets and minimal cut sets of this system, and provide an expression (do not simplify it!) for its structure function. (2.0)

• Minimal path sets

- $\mathcal{P}_1 = \{1, 2, 3\}$
- $\mathcal{P}_2 = \{1, 5, 6, 3\} = \{1, 3, 5, 6\}$
- $\mathcal{P}_3 = \{7, 4, 2, 3\} = \{2, 3, 4, 7\}$
- $\mathcal{P}_4 = \{7, 4, 5, 6, 3\} = \{3, 4, 5, 6, 7\}$
- $p^* = 4$  minimal path sets

• Minimal cut sets

- $\mathcal{K}_1 = \{3\}$
- $\mathcal{K}_2 = \{1, 7\}$
- $\mathcal{K}_3 = \{1, 4\}$
- $\mathcal{K}_4 = \{2, 5\}$
- $\mathcal{K}_5 = \{2, 6\}$
- $q = 5$  minimal cut sets

• Structure function

$$\begin{aligned} \phi(\underline{X}) &\stackrel{Th. 1.30}{=} 1 - \prod_{j=1}^{p^*} \left( 1 - \prod_{i \in \mathcal{P}_j} X_i \right) \\ &= 1 - (1 - X_1 X_2 X_3) \times (1 - X_1 X_3 X_5 X_6) \times (1 - X_2 X_3 X_4 X_7) \\ &\quad \times (1 - X_3 X_4 X_5 X_6 X_7) \end{aligned}$$

Obs. — Equivalently,

$$\begin{aligned} \phi(\underline{X}) &\stackrel{Th. 1.30}{=} \prod_{j=1}^q \left[ 1 - \prod_{i \in \mathcal{K}_j} (1 - X_i) \right] \\ &= [1 - (1 - X_3)] \times [1 - (1 - X_1)(1 - X_7)] \times [1 - (1 - X_1)(1 - X_4) \\ &\quad \times [1 - (1 - X_2)(1 - X_5)] \times [1 - (1 - X_2)(1 - X_6)]. \end{aligned}$$

(b) Admit that each of those 7 components are operational with probabilities  $p_i = 0.9$ ,  $i = 1, \dots, 7$ , and function independently. Obtain a lower and an upper bound (as strict as reasonably possible!) for the reliability of this system. (2.0)

• Reliability of the components

$$p_i = p = 0.9, \quad i = 1, \dots, 7$$

• Important

Since the 7 components form a coherent system and operate independently, we can apply Theorem 1.68.

• Lower bound for the reliability  $r(\underline{p})$

$$\begin{aligned} r(\underline{p}) &\stackrel{Th. 1.68}{\geq} \prod_{j=1}^q \left[ 1 - \prod_{i \in \mathcal{K}_j} (1 - p_i) \right] \\ &\stackrel{p_i=p}{=} \prod_{j=1}^q \left[ 1 - (1 - p)^{\#\mathcal{K}_j} \right] \\ &= [1 - (1 - p)] \times [1 - (1 - p)^2]^4 \\ &\stackrel{p=0.9}{=} 0.864536 \end{aligned}$$

• Upper bound for the reliability  $r(\underline{p})$

$$\begin{aligned} r(\underline{p}) &\stackrel{Th. 1.68}{\leq} 1 - \prod_{j=1, \dots, p^*} \left( 1 - \prod_{i \in \mathcal{P}_j} p_i \right) \\ &\stackrel{p_i=p}{=} 1 - \prod_{j=1, \dots, p^*} \left( 1 - p^{\#\mathcal{P}_j} \right) \\ &= 1 - (1 - p^3) \times (1 - p^4)^2 \times (1 - p^5) \\ &\stackrel{p=0.9}{=} 0.986875. \end{aligned}$$

(c) Assume that the times to failure (in  $10^2$  days) of those 7 components are i.i.d. random variables with a common IHRA distribution whose expected value is equal to  $\mu^* = 1$ .

(i) Determine a lower and an upper bound (as strict as reasonably possible!) for the expected time to failure of the communication system. (3.0)

• Individual durations, common stochastic ageing behavior and duration of the system

$$T_i \stackrel{i.i.d.}{\sim} IHRA, \quad i = 1, \dots, 7$$

$$E(T_i) = \mu^* = 1, \quad i = 1, \dots, 7$$

$T$  = duration of the communication system

- **Important**

Under these circumstances we can apply Theorem 3.69 to provide a lower and an upper bound for  $\mu = E(T)$ .

- **Lower bound for  $\mu = E(T)$**

$$\begin{aligned} \mu &\stackrel{Th. 3.69}{\geq} \max_{j=1, \dots, p^*} \left[ \left( \sum_{i \in \mathcal{P}_j} \mu_i^{-1} \right)^{-1} \right] \\ &\stackrel{\mu_i = \mu^*}{=} \max_{j=1, \dots, p^*} \left[ \left( \frac{\#\mathcal{P}_j}{\mu^*} \right)^{-1} \right] \\ &= \frac{\mu^*}{\min_{j=1, \dots, p^*} \#\mathcal{P}_j} \\ &\stackrel{\mu^* = 1}{=} \frac{1}{3}. \end{aligned}$$

- **Upper bound for  $\mu = E(T)$**

$$\begin{aligned} \mu &\stackrel{Th. 3.69}{\leq} \min_{j=1, \dots, q} \int_0^{+\infty} \left[ 1 - \prod_{i \in \mathcal{K}_j} (1 - e^{-t/\mu_i}) \right] dt \\ &\stackrel{\mu_i = \mu^*}{=} \min_{j=1, \dots, q} \int_0^{+\infty} \left[ 1 - (1 - e^{-t/\mu^*})^{\#\mathcal{K}_j} \right] dt \\ &\stackrel{\mu^* = 1}{=} \int_0^{+\infty} \left[ 1 - (1 - e^{-t})^{\min_{j=1, \dots, q} \#\mathcal{K}_j} \right] dt \\ &= \int_0^{+\infty} [1 - (1 - e^{-t})^1] dt \\ &= \int_0^{+\infty} e^{-t} dt \\ &= 1. \end{aligned}$$

(ii) Find an upper bound for the standard deviation of this time to failure. (1.5)

- **Upper bound for  $SD(T)$**

According to Table 3.2 the lifetime of a coherent system — with components with IHRA lifetimes — is also an IHRA r.v.

Consequently, we can apply Corollary 3.54 and add that

$$\begin{aligned} \frac{SD(T)}{E(T)} &\leq 1 \\ SD(T) &\leq E(T) = \mu \\ SD(T) &\stackrel{(i)}{\leq} 1 \end{aligned}$$

2. The logistic distribution has been used to model the time to failure  $T$  (in  $10^3$  km) of shock absorbers.<sup>1</sup> The corresponding c.d.f. is  $F(t) = \frac{1}{1 + e^{-\frac{t-\mu}{\sigma}}}$ , for  $-\infty < t < +\infty$  ( $-\infty < \mu < +\infty$  and  $\sigma > 0$ ).

(a) Derive the density, the reliability and the hazard rate functions of  $T$ .

<sup>1</sup>A shock absorber is a mechanical device designed to smooth out or damp shock impulse, and dissipate kinetic energy.

- **Time to failure and its c.d.f.**

$T$  = time to failure of (in  $10^3$  km) of a shock absorber

$T \sim \text{Logistic}(\mu, \sigma)$

$$F(t) = \frac{1}{1 + e^{-\frac{t-\mu}{\sigma}}}, \quad -\infty < t < +\infty \quad (-\infty < \mu < +\infty, \sigma > 0)$$

- **P.d.f. of  $T$**

$$\begin{aligned} f(t) &= \frac{dF(t)}{dt} \\ &= -\frac{\frac{de^{-\frac{t-\mu}{\sigma}}}{dt}}{\left(1 + e^{-\frac{t-\mu}{\sigma}}\right)^2} \\ &= \frac{1}{\sigma} \times \frac{e^{-\frac{t-\mu}{\sigma}}}{\left(1 + e^{-\frac{t-\mu}{\sigma}}\right)^2} \end{aligned}$$

- **Reliability function of  $T$**

$$\begin{aligned} R(t) &= 1 - F(t) \\ &= 1 - \frac{1}{1 + e^{-\frac{t-\mu}{\sigma}}} \\ &= \frac{e^{-\frac{t-\mu}{\sigma}}}{1 + e^{-\frac{t-\mu}{\sigma}}} \end{aligned}$$

- **Hazard rate function of  $T$**

$$\begin{aligned} \lambda(t) &= \frac{f(t)}{R(t)} \\ &= \frac{1}{\sigma} \times \frac{e^{-\frac{t-\mu}{\sigma}}}{\left(1 + e^{-\frac{t-\mu}{\sigma}}\right)^2} \\ &= \frac{e^{-\frac{t-\mu}{\sigma}}}{1 + e^{-\frac{t-\mu}{\sigma}}} \\ &= \frac{1}{\sigma} \times \frac{1}{1 + e^{-\frac{t-\mu}{\sigma}}}. \end{aligned}$$

(b) What can be said about the stochastic ageing character of  $T$ ? Can you predict the stochastic ageing character of the failure time of a parallel system with  $n$  components with failure times  $T_i \stackrel{i.i.d.}{\sim} T, i = 1, \dots, n$ ? (2.5)

- **Devising the stochastic ageing character of  $T$**

Since

$$\begin{aligned} \lambda(t) &= \frac{1}{\sigma} \times \frac{1}{1 + e^{-\frac{t-\mu}{\sigma}}} \\ &= \frac{1}{\sigma} \times F(t) \end{aligned}$$

is obviously an increasing function of  $t$  (because  $F(t)$  is...),

$$T \in \text{IHR}.$$

Although Def. 3.14, the notion of IHR distribution is valid for a r.v. taking values in  $\mathbb{R}$ , according to Barlow *et al.* (1963, p. 377).<sup>2</sup>

(2.0) <sup>2</sup>Barlow, R.E., Marshall, A.W. and Proschan, F. (1963). Properties of Probability Distributions with Monotone Hazard Rate. *The Annals of Mathematical Statistics* **34**, 375–389.

• **Devising the stochastic ageing character of  $T_{(n)}$**

$T_i$  = time to failure of the  $i^{th}$  component,  $i = 1, \dots, n$

$T_{(n)}$  = time to failure of the parallel system

According to Prop. 3.23, equation (3.14),

$$T_i \stackrel{i.i.d.}{\sim} IHR, i = 1, \dots, n \Rightarrow T_{(n)} \in IHR.$$

• **Obs.**

Even though Prop. 3.23 is stated for nonnegative r.v., result (3.14) is valid in the present case.

In fact,

$$\begin{aligned} F_{T_{(n)}}(t) &= [F(t)]^n \\ &= \left(1 + e^{-\frac{t-\mu}{\sigma}}\right)^{-n} \\ f_{T_{(n)}}(t) &= \frac{dF_{T_{(n)}}(t)}{dt} \\ &= nf(t)[F(t)]^{n-1} \\ &= \frac{n}{\sigma} \left(1 + e^{-\frac{t-\mu}{\sigma}}\right)^{-n-1} \\ \ln[f_{T_{(n)}}(t)] &= \ln(n) - \ln(\sigma) - (n+1) \ln\left(1 + e^{-\frac{t-\mu}{\sigma}}\right) \\ \frac{d^2 \log[f_{T_{(n)}}(t)]}{dt^2} &= \frac{d}{dt} \left[ \frac{1}{\sigma} \frac{(n+1)e^{-\frac{t-\mu}{\sigma}}}{1 + e^{-\frac{t-\mu}{\sigma}}} \right] \\ &= \frac{n+1}{\sigma} \frac{d}{dt} \left( \frac{1}{1 + e^{-\frac{t-\mu}{\sigma}}} \right) \\ &= -\frac{n+1}{\sigma^2} \frac{e^{-\frac{t-\mu}{\sigma}}}{\left(1 + e^{-\frac{t-\mu}{\sigma}}\right)^2} \\ &< 0, \end{aligned}$$

that is,  $f_{T_{(n)}}(t)$  is log-concave, thus,  $T_{(n)} \in ILR$ , according to Def. 3.32.<sup>3</sup> Consequently,

$$T_{(n)} \in ILR \stackrel{Prop. 3.36}{\Rightarrow} T_{(n)} \in IHR.$$

(c) Find a lower bound for the reliability for 5000km of the parallel system described in (b), when (2.0)

$\mu_i = \mu^* = 10$ ,  $\sigma = 1$  and  $n = 4$ . **Note:** Make use of Corollary 3.47 to derive a result similar to the one stated in Theorem 3.56.

• **Lower bound for  $R_{T_{(n)}}(t)$**

Since  $T_i \in IHR$ , we can apply Corollary 3.47, derive a result similar to the one stated in Theorem 3.56 and get:

$$\begin{aligned} R_{T_i}(t) &\geq e^{-t/\mu_i}, t < \mu_i \\ 1 - \prod_{i=1}^n [1 - R_{T_i}(t)] &\geq 1 - \prod_{i=1}^n \left(1 - e^{-t/\mu_i}\right), t < \min_{i=1, \dots, n} \mu_i \\ R_{T_{(n)}}(t) &\stackrel{\mu_i = \mu^*}{\geq} 1 - \left(1 - e^{-t/\mu^*}\right)^n, t < \mu^* \\ R_{T_{(4)}}(5) &\stackrel{\mu^* = 10, t = 5, n = 4}{\geq} 1 - \left(1 - e^{-5/10}\right)^4, t < 10 \\ &\geq 0.976031. \end{aligned}$$

<sup>3</sup>The notion of ILR distribution is also valid for r.v. taking values in  $\mathbb{R}$

3. 10 220 observations of the time  $T$  (in 1/5000 seconds) between  $\alpha$ -particle emissions of Americium-241 have been binned into intervals  $[t_j, t_{j+1})$ , as described in the following frequency table:

Interval	[0, 100)	[100, 300)	[300, 500)	[500, 700)	[700, 1000)	[1000, 2000)	[2000, 4000)	[4000, +∞)
Frequency	1609	2424	1770	1306	1213	1528	354	16

(a) Compute estimates of the density, the reliability and the hazard rate functions at  $t = 600$ . (1.5)

• **Non parametric estimates of  $f(t)$ ,  $R(t)$  and  $\lambda(t)$**

Let:

- $n$  = sample size;
- $N(t)$  = number of survivors at time  $t$ ;
- $[t_j, t_{j+1}) = j^{th}$  bin;
- $\Delta_j = t_{j+1} - t_j =$  range of the  $j^{th}$  bin.

According to Table 5.3, these estimates are, for  $t = 600 \in [t_4, t_5) = [500, 700)$ , given by:

$$\begin{aligned} \hat{f}(t) &= \frac{N(t_j) - N(t_{j+1})}{n \times \Delta t_j} \\ &= \frac{\text{number of failure in the } j^{th} \text{ bin}}{n \times \Delta t_j} \\ &\stackrel{j=4}{=} \frac{1306}{10220 \times (700 - 500)} \\ &\simeq 0.000639; \\ \hat{\lambda}(t) &= \frac{N(t_j) - N(t_{j+1})}{N(t_j) \times \Delta t_j} \\ &\stackrel{j=4}{=} \frac{1306}{[10220 - (1609 + 2424 + 1770)] \times 200} \\ &= \frac{1306}{(10220 - 5803) \times 200} \\ &= \frac{1306}{4417 \times 200} \\ &\simeq 0.001478. \end{aligned}$$

Since  $\hat{\lambda}(t) = \frac{\hat{f}(t)}{\hat{R}(t)}$  then

$$\begin{aligned} \hat{R}(t) &= \frac{\hat{f}(t)}{\hat{\lambda}(t)} \\ &= \frac{N(t_j)}{n} \\ &\stackrel{j=4}{=} \frac{4417}{10220} \\ &\simeq 0.432192. \end{aligned}$$

(b) A smaller sample, with 100 non censored observations, was analyzed in more detail and led to the exponential probability plot pictured above on the right. (1.5)

After having identified the abscissae and ordinates of this plot, comment on the goodness of fit of the proposed model and calculate a rough estimate of the expected value of  $T$ .

- **R.v.**

$T$  = time (in 1/5000 seconds) between  $\alpha$  - particle emissions of Americium-241

- **Conjectured model**

{Exponential( $\lambda$ ) :  $\lambda > 0$ }

- **Probability plot**

For any absolutely continuous model, we have

$$F_T(T_{(i)}) \sim \text{Beta}(i, n - i + 1).$$

Thus, by considering as an estimate of

$$p_i = F_T(t_{(i)}) = 1 - e^{-\lambda t_{(i)}}$$

the following expected value

$$\hat{p}_i = E[F_T(T_{(i)})] = E[\text{Beta}(i, n - i + 1)] = \frac{i}{n + 1},$$

we are bound to confront (indirectly and) graphically  $\hat{p}_i$  and  $F_T(t_{(i)})$ , that is,

$$\begin{aligned} \frac{i}{n + 1} &\rightarrow 1 - e^{-\lambda t_{(i)}} \\ 1 - \frac{i}{n + 1} &\rightarrow e^{-\lambda t_{(i)}} \\ -\frac{1}{\lambda} \ln \left( 1 - \frac{i}{n + 1} \right) &\rightarrow t_{(i)}. \end{aligned}$$

Consequently, the points in the exponential probability plot have abscissae and ordinates:

$$\left( -\ln \left( 1 - \frac{i}{n + 1} \right), t_{(i)} \right), i = 1, \dots, n.$$

- **Comment**

The points in the plot are set in an approximately linear fashion, hence the conjectured model fits very well to the data set.

- **Rough estimate of  $E(T) = \lambda^{-1}$**

It is obtained by determining a rough estimate of the slope ( $\lambda^{-1}$ ) of a line fitting the points of the probability plot, namely the ones closer to the origin:

$$\begin{aligned} \widetilde{\lambda^{-1}} &= \frac{500 - 0}{1 - 0} \\ &= 500. \end{aligned}$$

(c) Obtain a 95% confidence interval (CI) for the median of  $T$ , considering that  $\sum_{i=1}^{100} t_i = 61266.6$ . (2.0)

What were the underlying assumptions that allowed you to specify this quantile and obtain the CI?

- **Distribution assumption**

$T_i$  = time (in 1/5000 seconds) between the  $i^{th}$  and the  $(i + 1)^{th}$   $\alpha$  - particle emission of Americium-241

$T_i \stackrel{i.i.d.}{\sim} T \sim \text{Exponential}(\lambda), i = 1, \dots, n$

- **Life test**

Complete data is available!

$$\sum_{i=1}^{100} t_i = 61266.6$$

- **Another unknown parameter**

$$\begin{aligned} me &= \text{median of } T \\ &= F_T^{-1}(0.5) \\ &= -\frac{1}{\lambda} \ln(1 - 0.5) \end{aligned}$$

- $(1 - \alpha) \times 100\%$  **confidence interval (CI) for  $me$**

This CI can be obtained as follows:

- **Pivotal quantity**

$$Z = 2\lambda \sum_{i=1}^n T_i \sim \chi_{(2n)}^2 \text{ (check lecture note just before Exercise 5.26)}$$

- **Percentage points**

They are represented by  $a$  and  $b$ , balanced and such that  $P(a \leq Z \leq b) = 1 - \alpha$ , where  $\alpha = 0.05$ :

$$\begin{aligned} a &= F_{\chi_{(2n)}^2}^{-1}(\alpha/2) \\ &= F_{\chi_{(200)}^2}^{-1}(0.025) \\ &\stackrel{\text{table}}{=} 162.7 \\ b &= F_{\chi_{(2n)}^2}^{-1}(1 - \alpha/2) \\ &= F_{\chi_{(200)}^2}^{-1}(0.975) \\ &\stackrel{\text{table}}{=} 241.1 \end{aligned}$$

- **Inverting the inequality  $a \leq Z \leq b$**

Since  $me$  is a decreasing function of  $\lambda > 0$ , we can add that

$$\begin{aligned} P(a \leq Z \leq b) &= 1 - \alpha \\ P(a \leq 2\lambda \sum_{i=1}^n T_i \leq b) &= 1 - \alpha \end{aligned}$$

⋮

$$P\left(-\frac{2\ln(1-0.5)}{b} \sum_{i=1}^n T_i \leq -\frac{1}{\lambda} \ln(1-0.5) \leq -\frac{2\ln(1-0.5)}{a} \sum_{i=1}^n T_i\right) = 1 - \alpha.$$

- **CI**

$$\begin{aligned} CI_{95\%}(me) &= \left[ -\frac{2\ln(1-0.5)}{b} \sum_{i=1}^n t_i; -\frac{2\ln(1-0.5)}{a} \sum_{i=1}^n t_i \right] \\ &= \left[ -\frac{2\ln(1-0.5) \times 61266.6}{241.1}; -\frac{2\ln(1-0.5) \times 61266.6}{162.7} \right] \\ &\approx [352.275164; 522.025456]. \end{aligned}$$