

Reliability and Quality Control

t. Test

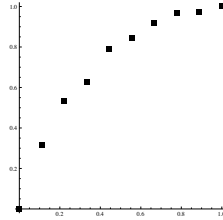
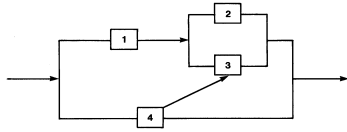
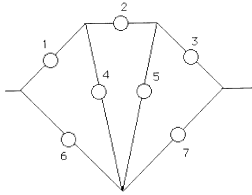
1st. Semester — 2011/12

ration: 1h30m

2011/11/05 — 8AM, Room P1

- Please justify your answers.
- This test has **one page** and **three questions**. The total of points is **20.0**.

1. Admit that a transponder¹ crucially depends on a diamond structure (pictured on the left) with 7 components.



Diamond structure (left, question 1); crosslinked system (center, question 2); TTT plot (right, question 3).

(a) Prove that component 4 is not irrelevant, and provide an expression (do not simplify it!) for the structure function of the diamond structure of the transponder. (2)

• **Relevance of component 4**

Component 4 is not irrelevant because there is at least a state vector \underline{x} such that:

$$\phi(0_4, \underline{x}) \neq \phi(1_4, \underline{x}).$$

In fact, for

$$\underline{x} = (1, 0, 0, 1, 0, 0, 1),$$

we get

$$\begin{aligned} \phi(0_4, \underline{x}) &= \phi(1, 0, 0, 0, 0, 0, 1) = 0 \\ &\neq \phi(1_4, \underline{x}) = \phi(1, 0, 0, 1, 0, 0, 1) = 1, \end{aligned}$$

because the system does not function when only components 1 and 7 operate, whereas it operates with components 1, 4 and 7 functioning.

• **Minimal path sets**

- $\mathcal{P}_1 = \{1, 2, 3\}$
- $\mathcal{P}_2 = \{1, 4, 7\}$
- $\mathcal{P}_3 = \{1, 4, 5, 3\} = \{1, 3, 4, 5\}$
- $\mathcal{P}_4 = \{1, 2, 5, 7\}$
- $\mathcal{P}_5 = \{6, 7\}$
- $\mathcal{P}_6 = \{6, 4, 2, 3\} = \{2, 3, 4, 6\}$
- $\mathcal{P}_7 = \{6, 5, 3\} = \{3, 5, 6\}$
- $p^* = 7$ minimal path sets

¹Aircraft have transponders to assist in identifying them on radar and on other aircraft's collision avoidance systems.

• **Structure function**

$$\begin{aligned} \phi(\underline{X}) &\stackrel{T1.30}{=} 1 - \prod_{j=1}^{p^*} \left(1 - \prod_{i \in \mathcal{P}_j} X_i \right) \\ &= 1 - (1 - X_1 X_2 X_3)(1 - X_1 X_4 X_7)(1 - X_1 X_3 X_4 X_5)(1 - X_1 X_2 X_5 X_7) \\ &\quad \times (1 - X_6 X_7)(1 - X_2 X_3 X_4 X_6)(1 - X_3 X_5 X_6). \end{aligned}$$

(b) Now, admit that each of those 7 components have reliability $p_i = p = 0.975, i = 1, \dots, 7$, and (2) operate in an independent fashion. Obtain a lower and an upper bound (as strict as possible) for the reliability of the diamond structure.

• **Components**

$$p_i = p = 0.975, i = 1, \dots, 7$$

Since the 7 components form a coherent system and operate independently, we can apply Theorem 1.68.

• **Minimal cut sets**

- $\mathcal{K}_1 = \{1, 6\}$
- $\mathcal{K}_2 = \{3, 7\}$
- $\mathcal{K}_3 = \{2, 4, 6\}$
- $\mathcal{K}_4 = \{1, 4, 5, 7\}$
- $\mathcal{K}_5 = \{3, 4, 5, 6\}$
- $\mathcal{K}_6 = \{2, 5, 7\}$
- $q = 6$ minimal cut sets

• **Lower bound for the reliability $r(p)$**

$$\begin{aligned} r(p) &\stackrel{T1.68}{\geq} \prod_{j=1}^q \left[1 - \prod_{i \in \mathcal{K}_j} (1 - p_i) \right] \\ &\stackrel{p_i=p}{=} \prod_{j=1}^q \left[1 - (1 - p)^{\#\mathcal{K}_j} \right] \\ &= \left[1 - (1 - p)^2 \right]^2 \times \left[1 - (1 - p)^3 \right]^2 \times \left[1 - (1 - p)^4 \right]^2 \\ &\stackrel{p=0.975}{=} 0.998718. \end{aligned}$$

• **Upper bound for the reliability**

$$\begin{aligned} r(p) &\stackrel{T1.68}{\leq} 1 - \prod_{j=1}^{p^*} \left(1 - \prod_{i \in \mathcal{P}_j} p_i \right) \\ &\stackrel{p_i=p}{=} 1 - \prod_{j=1}^{p^*} \left(1 - p^{\#\mathcal{P}_j} \right) \\ &= 1 - (1 - p^2) \times (1 - p^3)^3 \times (1 - p^4)^3 \\ &\stackrel{p=0.975}{=} 0.999999982. \end{aligned}$$

• **Obs.**

Theorem 1.70 (Min-Max for positively associated) leads to a worse lower bound:

$$r(p) \stackrel{T1.70}{\geq} \max_{j=1, \dots, p^*} \prod_{i \in \mathcal{P}_j} p_i$$

$$\begin{aligned}
& \stackrel{p_i=p}{=} \max_{j=1,\dots,p^*} p^{\#\mathcal{P}_j} \\
& = p^{\min_{j=1,\dots,p^*} \#\mathcal{P}_j} \\
& = p^2 \\
& \stackrel{p=0.975}{=} 0.950625.
\end{aligned}$$

A better upper bound can be obtained by using Theorem 1.70 (Min-Max):

$$\begin{aligned}
r(\underline{p}) & \stackrel{T1.70}{\leq} \min_{j=1,\dots,q} \left[1 - \prod_{i \in \mathcal{K}_j} (1 - p_i) \right] \\
& = \min_{j=1,\dots,q} \left[1 - (1 - p)^{\#\mathcal{K}_j} \right] \\
& = 1 - (1 - p)^{\min_{j=1,\dots,q} \#\mathcal{K}_j} \\
& = 1 - (1 - p)^2 \\
& \stackrel{p=0.975}{=} 0.999375.
\end{aligned}$$

- (c) Assume now that the durations (in 10^3 days) of the 7 components are positively associated random variables with common Weibull distribution with scale parameter $\delta = 1$ and shape parameter $\alpha = 2$. Determine a lower and an upper bound (as strict as possible) for the reliability function of the same structure for a period of 2 years.

• **Individual durations, common distribution and duration of the system**

T_i , $i = 1, \dots, 7$ positively associated r.v.

$T_i \stackrel{i.i.d.}{\sim} \text{Weibull}(\delta = 1, \alpha = 2)$

$R_i(t) = R(t) = e^{-t^2}$, $t \geq 0$

T = duration of the system

Under these circumstances we can apply Theorem 2.22 to provide a lower and an upper bound for $R_T(t)$.

• **Lower bound for the reliability function $R_T(t)$**

$$\begin{aligned}
R_T(t) & \stackrel{T2.22}{\geq} \max_{j=1,\dots,p^*} \left[\prod_{i \in \mathcal{P}_j} R_i(t) \right] \\
& \stackrel{R_i(t)=R(t)}{=} \max_{j=1,\dots,p^*} [R_i(t)]^{\#\mathcal{P}_j} \\
& = [R(t)]^{\min_{j=1,\dots,p^*} \#\mathcal{P}_j} \\
& = [R(t)]^2 \\
& = \left(e^{-t^2} \right)^2 \\
& \stackrel{t=\frac{2 \times 365}{1000}}{=} e^{-2 \times \left(\frac{2 \times 365}{1000} \right)^2} \\
& \simeq 0.344452.
\end{aligned}$$

• **Upper bound for the reliability function $R_T(t)$**

$$\begin{aligned}
R_T(t) & \stackrel{T2.22}{\leq} \min_{j=1,\dots,q} \left\{ 1 - \prod_{i \in \mathcal{K}_j} [1 - R_i(t)] \right\} \\
& \stackrel{R_i(t)=R(t)}{=} \min_{j=1,\dots,q} \left\{ 1 - [1 - R(t)]^{\#\mathcal{K}_j} \right\} \\
& = 1 - [1 - R(t)]^{\min_{j=1,\dots,q} \#\mathcal{K}_j}
\end{aligned}$$

$$\begin{aligned}
& = 1 - [1 - R(t)]^2 \\
& = 1 - \left(1 - e^{-t^2} \right)^2 \\
& \stackrel{t=\frac{2 \times 365}{1000}}{=} 1 - \left[1 - e^{-\left(\frac{2 \times 365}{1000} \right)^2} \right]^2 \\
& \simeq 0.829349.
\end{aligned}$$

2. A crosslinked system comprises 4 silicon photodiode² detectors, as pictured above in the center. The durations (in 10^4 hours) of these 4 detectors, T_i ($i = 1, \dots, 4$) are i.i.d. random variables with common reliability function $R(t) = t^{-3}$, for $t \geq 1$, and $R(t) = 1$, for $t < 1$.

- (a) Obtain the reliability function of the crosslinked system for a period of 87600 hours. (3)

• **Individual durations and common reliability function**

T_i , $i = 1, \dots, 4$, i.i.d. r.v. with reliability function

$$R_{T_i}(t) = R(t) = \begin{cases} 1, & t < 1 \\ t^{-3}, & t \geq 1 \end{cases}$$

• **Duration of the system**

$T = \max\{\min\{T_1, \max\{T_2, T_3\}\}, T_4\}$

• **Reliability function of $\max\{T_2, T_3\}$**

According to Example 2.6, it is equal to

$$R_{\max\{T_2, T_3\}}(t) \stackrel{R_{T_i}(t)=R(t)}{=} 1 - [1 - R(t)]^2$$

• **Reliability function of $\min\{T_1, \max\{T_2, T_3\}\}$**

Following Example 2.5, we get

$$R_{\min\{T_1, \max\{T_2, T_3\}\}}(t) \stackrel{R_{T_i}(t)=R(t)}{=} R_{T_1}(t) \times R_{\max\{T_2, T_3\}}(t) = R(t) \times \left\{ 1 - [1 - R(t)]^2 \right\}$$

• **Reliability function of T**

$$\begin{aligned}
R_T(t) & = R_{\max\{\min\{T_1, \max\{T_2, T_3\}\}, T_4\}}(t) \\
& = 1 - \left[1 - R_{\min\{T_1, \max\{T_2, T_3\}\}}(t) \right] \times [1 - R_{T_4}(t)] \\
& \stackrel{R_{T_i}(t)=R(t)}{=} 1 - \left(1 - R(t) \times \left\{ 1 - [1 - R(t)]^2 \right\} \right) \times [1 - R(t)]
\end{aligned}$$

• **Reliability for a period of 87600 hours**

$$\begin{aligned}
R_T(8.76) & = 1 - \left(1 - R(8.76) \times \left\{ 1 - [1 - R(8.76)]^2 \right\} \right) \times [1 - R(8.76)] \\
& = 1 - \left\{ 1 - 8.76^{-3} \times \left[1 - \left(1 - 8.76^{-3} \right)^2 \right] \right\} \times \left(1 - 8.76^{-3} \right) \\
& \simeq 0.001492.
\end{aligned}$$

Alternative method

• **Individual durations and common reliability function**

T_i , $i = 1, \dots, 7$, i.i.d. r.v. with reliability function

$$R_i(t) = R(t) = \begin{cases} 1, & t < 1 \\ t^{-3}, & t \geq 1 \end{cases}$$

²A photodiode exhibits sensitivity to light, for instance by varying its electrical resistance like a photoresistor.

- **Minimal path sets**

$$\mathcal{P}_1 = \{1, 2\}$$

$$\mathcal{P}_2 = \{1, 3\}$$

$$\mathcal{P}_3 = \{4\}$$

- **Structure function**

$$\begin{aligned} \phi(\underline{X}) &\stackrel{T1.30}{=} 1 - \prod_{j=1}^{p^*} \left(1 - \prod_{i \in \mathcal{P}_j} X_i \right) \\ &= 1 - (1 - X_1 X_2)(1 - X_1 X_3)(1 - X_4) \\ &= 1 - (1 - X_1 X_2 - X_1 X_3 + X_1^2 X_2 X_3)(1 - X_4) \\ X_1^2 &\stackrel{=st X_1}{=} 1 - (1 - X_1 X_2 - X_1 X_3 + X_1 X_2 X_3 - X_4 + X_1 X_2 X_4 + X_1 X_3 X_4 \\ &\quad - X_1 X_2 X_3 X_4) \\ &= X_4 + X_1 X_2 + X_1 X_3 - X_1 X_2 X_3 - X_1 X_2 X_4 - X_1 X_3 X_4 + X_1 X_2 X_3 X_4. \end{aligned}$$

- **Reliability**

Since $\underline{X} = (X_1, \dots, X_4)$, where $X_i \stackrel{indep}{\sim} \text{Bernoulli}(p_i)$, $i = 1, 2, 3, 4$, we get:

$$\begin{aligned} r(\underline{p}) &= r(p_1, \dots, p_4) \\ &= E[\phi(\underline{X})] \\ &= p_4 + p_1 p_2 + p_1 p_3 - p_1 p_2 p_3 - p_1 p_2 p_4 - p_1 p_3 p_4 + p_1 p_2 p_3 p_4 \\ p_i &\stackrel{=p}{=} p + 2p^2 - 3p^3 + p^4 \end{aligned}$$

- **Reliability function**

Considering T the duration of the crosslinked system, we have:

$$\begin{aligned} R_T(t) &= P(T > t) \\ &\stackrel{N2.8}{=} r(R_1(t), \dots, R_4(t)) \\ &= r(R(t), \dots, R(t)) \\ &= R(t) + 2[R(t)]^2 - 3[R(t)]^3 + [R(t)]^4 \\ R(t) &\stackrel{=t^{-3}}{=} t^{-3} + 2(t^{-3})^2 - 3(t^{-3})^3 + (t^{-3})^4 \\ t &\stackrel{=8.76}{=} 0.001492. \end{aligned}$$

(b) Are the durations T_i DHRA? What can be said about the stochastic ageing of the duration of the crosslinked system? (3)

- **Individual durations and common reliability function**

T_i , $i = 1, \dots, 7$, i.i.d. r.v. with reliability function

$$R_i(t) = R(t) = \begin{cases} 1, & t < 1 \\ t^{-3}, & t \geq 1 \end{cases}$$

- **Common p.d.f.**

$$\begin{aligned} f(t) &= -\frac{dR(t)}{dt} \\ &= \begin{cases} 0, & t < 1 \\ 3t^{-4}, & t \geq 1 \end{cases} \end{aligned}$$

- **Common hazard rate function**

$$\lambda(t) = \frac{f(t)}{R(t)}$$

$$= \begin{cases} 0, & t < 1 \\ \frac{3t^{-4}}{t^{-3}} = \frac{3}{t}, & t \geq 1 \end{cases}$$

- **Obs.**

$T_i \notin \text{DHR}$ because $\lambda(t)$ is not a decreasing function for $t \geq 0$ (even though it is decreasing for $t \geq 1$).

- **Investigating the DHRA character of the T_i 's**

$$\begin{aligned} \frac{1}{t} \Lambda(t) &= \frac{1}{t} \int_0^t \lambda(u) du \\ &= \begin{cases} 0, & t < 1 \\ \frac{1}{t} \int_1^t \frac{3}{u} du = \frac{3 \ln(t)}{t}, & t \geq 1 \end{cases} \\ \frac{d}{dt} \frac{1}{t} \Lambda(t) &= \frac{3}{t^2} [1 - \ln(t)], t \geq 1 \\ &= \begin{cases} \geq 0, & 1 \leq t \leq e \\ \leq 0, & t \geq e \end{cases} \end{aligned}$$

- **Conclusion**

$\frac{1}{t} \Lambda(t)$ is not a monotonous function for $t \geq 0$, thus $T_i \notin \text{DHRA}$.

- **Stochastic ageing of T**

According to Table 3.2, the DHRA property of the components of a system is not necessarily preserved after the formation of a coherent system. Thus, even if the T_i were DHRA we could not add anything about the stochastic ageing of T , the duration of the (coherent) crosslinked system.

(c) Calculate the common value of $\mu_i = E(T_i) = \mu^*$ and obtain a lower limit for the expected value of the duration of the parallel sub-system with components 2 and 3, falsely assuming that $T_i \in \text{DHRA}$. (2)

- **Common expected value**

$$\begin{aligned} \mu^* &\stackrel{T_i \geq 0}{=} \int_0^{+\infty} R(t) dt \\ &= \int_0^1 1 dt + \int_1^{+\infty} t^{-3} dt \\ &= 1 - \frac{t^{-2}}{2} \Big|_1^{+\infty} \\ &= \frac{3}{2} \end{aligned}$$

- **Lower bound for $\mu_P = E(\max T_2, T_3)$**

Since T_2 and T_3 are independent r.v. (therefore positively associated) and we are falsely assuming that they are both DHRA, we can apply Theorem 3.64 (Equation (3.57) with the inequality reversed) and get

$$\begin{aligned} \mu_P &= E(\max T_2, T_3) \\ &\geq \int_0^{+\infty} \left[1 - \prod_{i=1}^n (1 - e^{-t/\mu_i}) \right] dt \\ n=2, \mu_i &\stackrel{= \mu^* = 3/2}{=} \int_0^{+\infty} \left[1 - (1 - e^{-2t/3})^2 \right] dt \\ &= \int_0^{+\infty} (2e^{-2t/3} - e^{-4t/3}) dt \end{aligned}$$

$$\begin{aligned}
&= -3e^{-2t/3}\Big|_0^{+\infty} + \frac{3}{4}e^{-4t/3}\Big|_0^{+\infty} \\
&= 3 - \frac{3}{4} \\
&= \frac{9}{4}.
\end{aligned}$$

3. (a) A sample of 9 specimens of a titanium alloy were subjected to a fatigue test to determine time to crack initiation. The observed times of crack initiation (in units of 10^3 cycles) were 18, 32, 39, 53, 59, 68, 77, 78, 93, and the TTT plot pictured above on the right.

i) Exemplify the obtention of the TTT plot, by using just 4 points and the fact that the total time in test is 517 (in units of 10^3 cycles).

• **Failure times**

T_i = time (in units of 10^3) of crack initiation of specimen i , $i = 1, \dots, 9$

• **Complete data**

$\underline{t} = (18, 32, 39, 53, 59, 68, 77, 78, 93)$

• **Total time on test up to time $t_{(i)}$**

$$\tau(t_{(i)}) = \sum_{j=1}^i (n - j + 1) [t_{(j)} - t_{(j-1)}]$$

• **Abcissae of the TTT plot**

$\frac{i}{n}$, $i = 0, 1, \dots, n$

• **Ordinates of the TTT plot**

$\frac{\tau(t_{(i)})}{\tau(t_{(n)})}$, $i = 1, \dots, n$, where $\tau(t_{(n)}) = 517$; equal to 0, for $i = 0$.

• **Four points of the TTT plot**

i	$\frac{i}{n}$	$\tau(t_{(i)}) = \sum_{j=1}^i (n - j + 1) [t_{(j)} - t_{(j-1)}]$	$\frac{\tau(t_{(i)})}{\tau(t_{(n)})}$
0	0	0	0
1	$\frac{1}{9} = 0.(1)$	$(9 - 1 + 1) \times 18 = 162$	$\frac{162}{517} \approx 0.313$
2	$\frac{2}{9} = 0.(2)$	$162 + (9 - 2 + 1) \times (32 - 18) = 274$	$\frac{274}{517} \approx 0.530$
3	$\frac{3}{9} = 0.(3)$	$274 + (9 - 3 + 1) \times (39 - 32) = 323$	$\frac{323}{517} \approx 0.625$

ii) What sort of stochasting ageing does this TTT plot suggest for the time to crack initiation? (0)

• **Suggested stochastic ageing**

The TTT plot is concave. This suggests a *IHR* behavior of the time to crack initiation.

(b) A life test for a new insulating material used 25 specimens. The specimens were tested simultaneously at 30kV, the test was run until 15 of the specimens failed, and the ordered failure times ($t_{(i)}$) recorded as: 1.08, 12.20, 17.80, 19.10, 26.00, 27.90, 28.20, 32.20, 35.90, 43.50, 44.00, 45.20, 45.70, 46.30, 47.80 (with $\sum_{i=1}^{15} t_{(i)} = 472.88$).

After having specified some convenient distribution assumption, obtain a 95% confidence interval for the 80% quantile of the failure time (T) distribution, $F_T^{-1}(0.80)$.

• **Distribution assumption**

$T_i \stackrel{i.i.d.}{\sim} \text{Exponential}(\lambda)$, $i = 1, \dots, 25$

• **Life test**

Since the end of the test was determined by $r = 15^{\text{th}}$ failure and nothing in this exercise suggests that the $n = 25$ specimens were replaced during the life test (they “were tested simultaneously”), we are dealing with a

◦ Type II/item censored testing without replacement.

• **Unknown parameter**

λ

• **Censored data**

$(t_{(1)}, \dots, t_{(r)}) = (1.08, 12.20, \dots, 46.30, 47.8015)$

$n = 25$

$r = 15$

$\sum_{i=1}^{15} t_{(i)} = 472.88$

• **Cumulative total time in test**

$$\begin{aligned}
\tilde{t} &\stackrel{D^{5,17}}{=} \sum_{i=1}^r t_{(i)} + (n - r) \times t_{(r)} \\
&= 472.88 + (25 - 15) \times 47.80 \\
&= 950.88
\end{aligned}$$

• **Confidence interval for λ**

$$\begin{aligned}
CI_{(1-\alpha) \times 100\%}(\lambda) &= [\lambda_L; \lambda_U] \\
&= \left[\frac{F_{\chi^2(2r)}(\alpha/2)}{2 \times \tilde{t}}; \frac{F_{\chi^2(2r)}(1 - \alpha/2)}{2 \times \tilde{t}} \right] \\
CI_{95\%}(\lambda) &= \left[\frac{F_{\chi^2(30)}(0.025)}{2 \times 950.88}; \frac{F_{\chi^2(30)}(0.975)}{2 \times 950.88} \right] \\
&= \left[\frac{16.79}{1901.76}; \frac{46.98}{1901.76} \right] \\
&\approx [0.008829; 0.024703]
\end{aligned}$$

• **Another unknown parameter**

$F_T^{-1}(0.80) = -\frac{1}{\lambda} \ln(1 - 0.80)$, which is a decreasing function of $\lambda > 0$.

• **Confidence interval for $F_T^{-1}(0.80)$**

$$\begin{aligned}
CI_{95\%}(F_T^{-1}(0.80)) &= \left[\frac{1}{\lambda_U} \ln(1 - 0.80); \frac{1}{\lambda_L} \ln(1 - 0.80) \right] \\
&\approx [65.150376; 182.296882].
\end{aligned}$$