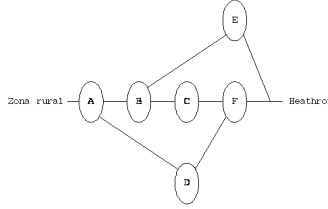


1. O esquema abaixo descreve as etapas de uma deslocação em transportes públicos de uma zona rural do sul da Inglaterra ao aeroporto de Heathrow. Há a possibilidade de ocorrência de avaria em cada uma das etapas da deslocação, contribuindo assim para que um passageiro perca o seu voo.

Considere que os transportes B, D, E e F (A e C, resp.) possuem probabilidade de avaria q (2q, resp.) e funcionam de modo independente.



- (a) Identifique as fiabilidades dos transportes, os caminhos mínimos, os cortes mínimos e a função estrutura.

(2.5)

• Reliabilities of the components/transportes

$$p_i = 1 - P(\text{breakdown of transport } i), i = A, \dots, F$$

$$p_B = p_D = p_E = p_F = 1 - q$$

$$p_A = p_C = 1 - 2q$$

• Minimal path sets

$$\mathcal{P}_1 = \{A, B, E\}$$

$$\mathcal{P}_2 = \{A, D, F\}$$

$$\mathcal{P}_3 = \{A, B, C, F\}$$

$$p^* = 3 \text{ minimal path sets}$$

• Minimal cut sets

$$\mathcal{K}_1 = \{A\}$$

$$\mathcal{K}_2 = \{B, D\}$$

$$\mathcal{K}_3 = \{B, F\}$$

$$\mathcal{K}_4 = \{C, D, E\}$$

$$\mathcal{K}_5 = \{E, F\}$$

$$q^* = 5 \text{ minimal cut sets}$$

• Structure function

By considering  $X_i \sim \text{Bernoulli}(p_i)$ ,  $i = A, \dots, F$  and applying result (1.13) or (1.14), we can conclude that the structure function of this system equals:

$$\phi(\underline{X}) \stackrel{(1.13)}{=} 1 - \prod_{j=1}^{p^*} \left( 1 - \prod_{i \in \mathcal{P}_j} X_i \right)$$

$$\begin{aligned} &= 1 - (1 - X_A X_B X_E)(1 - X_A X_D X_F)(1 - X_A X_B X_C X_F) \\ (1.14) \quad &\prod_{j=1}^{p^*} \left[ 1 - \prod_{i \in \mathcal{K}_j} (1 - X_i) \right] \\ &= [1 - (1 - X_A)] \times [1 - (1 - X_B)(1 - X_D)] \times [1 - (1 - X_B)(1 - X_F)] \\ &\quad \times [1 - (1 - X_C)(1 - X_D)(1 - X_E)] \times [1 - (1 - X_E)(1 - X_F)]. \end{aligned}$$

- (b) Calcule um par de limites inferior e superior o mais estritos possível para a fiabilidade desta deslocação a Heathrow.

(2.0)

• Bounds for the reliability  $r(\underline{p})$

Since the components form a coherent system and operate in an independent fashion, we can apply Theorem 1.68, use the fact that  $p_A = p_C = 1 - 2q$  and  $p_B = p_D = p_E = p_F = 1 - q$  and successively get:

– Lower bound

$$\begin{aligned} r(\underline{p}) &\geq \prod_{j=1}^{q^*} \left[ 1 - \prod_{i \in \mathcal{K}_j} (1 - p_i) \right] \\ &= [1 - (1 - p_A)] \times [1 - (1 - p_B)(1 - p_D)] \times [1 - (1 - p_B)(1 - p_F)] \\ &\quad \times [1 - (1 - p_C)(1 - p_D)(1 - p_E)] \times [1 - (1 - p_E)(1 - p_F)] \\ &= (1 - 2q) \times (1 - q^2) \times (1 - q^2) \times (1 - 2qq^2) \times (1 - q^2) \\ &= (1 - 2q) \times (1 - q^2)^3 \times (1 - 2qq^2) \end{aligned}$$

– Upper bound

$$\begin{aligned} r(\underline{p}) &\leq 1 - \prod_{j=1}^{p^*} \left( 1 - \prod_{i \in \mathcal{P}_j} p_i \right) \\ &= 1 - (1 - p_A p_B p_E)(1 - p_A p_D p_F)(1 - p_A p_B p_C p_F) \\ &= 1 - [1 - (1 - 2q)(1 - q)^2] \times [1 - (1 - 2q)(1 - q)^2] \\ &\quad \times [1 - (1 - 2q)^2(1 - q)^2]. \end{aligned}$$

2. Um veículo pesado possui 2 eixos, com 6 pneus cada (3 de cada lado). Este veículo opera quando os dois eixos estão a funcionar. Um eixo fica inoperacional se mais de um dos 3 pneus de cada lado estiver furado.

- (a) Obtenha um limite inferior para a fiabilidade do veículo, assumindo que os 12 pneus do veículo funcionam de forma associada (positiva) e que a fiabilidade de cada pneu é de 97.5%.

(3.0)

• System

The vehicle described in the text is a system with the following characteristics:

- Each SIDE OF THE AXIS corresponds to a 2 – out – of – 3 system because each axis is non operational if more than one of the 3 tires is non operational, that is, the system is operational if at least 2 of the 3 tires is operational;
- each AXIS is nothing but two 2 – out – of – 3 sub-systems put in series;
- the VEHICLE only operates when both axes are operational, therefore the vehicle corresponds to 2 – out – of – 3 sub-systems put in series.

- **Reliability of the components of each 2 – out – of – 3 sub-system**

$$p_i = p^* = 0.975, \quad i = 1, 2, 3$$

- **Lower bound for the reliability of each 2 – out – of – 3 sub-system**

Since the 3 components form a coherent sub-system and operate in a positively associated fashion, we can apply Theorem 1.70, namely result (1.42), after having identified the minimal path sets.

- **Minimal path sets**

$$\mathcal{P}_1 = \{1, 2\}$$

$$\mathcal{P}_2 = \{1, 3\}$$

$$\mathcal{P}_3 = \{2, 3\}$$

$$p^* = 3 \text{ minimal path sets}$$

- **Lower bound for the reliability**

$$\begin{aligned} r_{2\text{-out-of-3}}(\underline{p}) &\stackrel{(1.42)}{\geq} \max_{j=1, \dots, p^*} \prod_{i \in \mathcal{P}_j} p_i \\ &\stackrel{p_i=p}{=} \max_{j=1, \dots, p^*} p^{\#\mathcal{P}_j} \\ &\stackrel{\#\mathcal{P}_j=2, \forall j}{=} p^2 \\ &\stackrel{p=0.975}{=} 0.975^2 \\ &= 0.950625. \end{aligned}$$

- **Lower bound for the reliability of the vehicle**

Now, we can capitalize on the previous bound for the reliability of each of the four sub-systems and apply Theorem 1.65 to provide the requested lower bound or the reliability of the vehicle:

$$\begin{aligned} r_{vehicle}(\underline{p}) &\stackrel{(1.34)}{\geq} \prod_{i=1}^4 r_{2\text{-out-of-3}, i}(\underline{p}) \\ &= 0.950625^4 \\ &= 0.816652. \end{aligned}$$

- (b) *Considere agora que os “tempos” até que os pneus fiquem furados (em milhares de Km) são i.i.d. com distribuição Weibull com parâmetro de escala  $\delta = 1$  e de forma  $\alpha = 2$ . Obtenha a função de fiabilidade da vida do veículo para uma deslocação de 400 Km.* (2.5)

- **Individual durations of the components of each 2 – out – of – 3 sub-system**

$T_i$  *i.i.d.* Weibull( $\delta = 1, \alpha = 2$ ),  $i = 1, 2, 3$

$$F_i(t) = F(t) = 1 - e^{-t^2}, \quad t \geq 0$$

- **Duration of each 2 – out – of – 3 sub-system**

$S_j$  = duration of the  $j^{th}$  2 – out – of – 3sub-system,  $j = 1, \dots, 4$

$$S_i \stackrel{(2.6)}{=} T_{(n-k+1)} \stackrel{n=3, k=2}{=} T_{(2)}$$

- **Reliability function of  $S_j$**

For  $j = 1, \dots, 4$ ,

$$\begin{aligned} R_{S_j}(t) &\stackrel{(2.8)}{=} F_{Binomial(3, F(t))(3-2)} \\ &= \sum_{m=0}^1 \binom{3}{m} (1 - e^{-t^2})^m [1 - (1 - e^{-t^2})]^{3-m} \end{aligned}$$

$$\begin{aligned} &= e^{-3t^2} + 3(1 - e^{-t^2})e^{-2t^2} \\ &\stackrel{t=0.4}{\simeq} 0.94088 \end{aligned}$$

- **Duration of the vehicle**

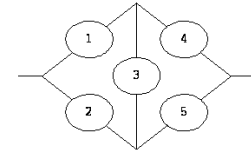
$$S_{vehicle} = \min_{j=1, \dots, 4} S_j$$

- **Reliability function of  $S_{vehicle}$**

$$\begin{aligned} R_{S_{vehicle}}(t) &\stackrel{(2.3)}{=} \prod_{j=1}^4 R_{S_j}(t) \\ &= [e^{-3t^2} + 3(1 - e^{-t^2})e^{-2t^2}]^4 \\ &\stackrel{t=0.4}{\simeq} 0.94088^4 \\ &\simeq 0.783678. \end{aligned}$$

3. *Um sistema em ponte possui componentes, com durações (em horas) i.i.d. e função taxa de falha comum*

$$\lambda(t) = \begin{cases} t, & 0 < t \leq 1.5 \\ 3 - t, & 1.5 < t \leq 2 \\ t - 1, & t > 2. \end{cases}$$



- (a) *Qual o comportamento monótono da função taxa de falha das durações das componentes e da duração da estrutura? Justifique.* (3.0)

- **Individual durations and common hazard rate function**

$T_i$ ,  $i = 1, \dots, 5$ , i.i.d. r.v. with hazard rate function  $\lambda(t)$ .

- **Stochastic aging character of  $T_i$**

$\lambda(t)$  is not a monotone (or monotonic) function. Thus,  $T_i \notin IHR$  or  $T_i \notin DHR$ . However,

$$\begin{aligned} \frac{1}{t}\Lambda(t) &= \frac{1}{t} \int_0^t \lambda(u) du \\ &= \frac{1}{t} \times \begin{cases} 0, & t < 0 \\ \int_0^t u du, & 0 \leq t \leq 1.5 \\ \int_0^{\frac{t}{2}} \frac{0}{1.5} u du + \int_{1.5}^t (3 - u) du, & 1.5 < t \leq 2 \\ \int_0^{\frac{t}{2}} \frac{0}{1.5} u du + \int_{1.5}^2 (3 - u) du + \int_2^t (u - 1) du, & t > 2 \end{cases} \\ &= \frac{1}{t} \times \begin{cases} 0, & t < 0 \\ \frac{t^2}{2}, & 0 \leq t \leq 1.5 \\ \frac{1.5^2}{2} + \left(3u - \frac{u^2}{2}\right) \Big|_{1.5}^t, & 1.5 < t \leq 2 \\ -2.25 + 3 \times 2 - \frac{2^2}{2} + [(t^2 - t) - (2^2 - 2)], & t > 2 \end{cases} \\ &\dots \end{aligned}$$

$$= \frac{1}{t} \times \begin{cases} 0, & t < 0 \\ \frac{t^2}{2}, & 0 \leq t \leq 1.5 \\ -2.25 + 3t - \frac{t^2}{2}, & 1.5 < t \leq 2 \\ \frac{t^2}{2} - t + 1.75, & t > 2 \end{cases}$$

$$\frac{d}{dt} \frac{1}{t} \Lambda(t) = \begin{cases} \frac{1}{2}, & 0 \leq t \leq 1.5 \\ \frac{2.25}{t^2} - \frac{1}{2}, & 1.5 < t \leq 2 \\ \frac{1}{2} - \frac{1.75}{t^2}, & t > 2. \end{cases}$$

Please note that:

- $\frac{1}{2} > 0$ ;
- $\frac{2.25}{t^2} - \frac{1}{2}$  is a decreasing function, thus, the minimum value is this function in  $(1.5, 2]$  is  $\frac{2.25}{2^2} - \frac{1}{2} = 0.0625 > 0$ ;
- $\frac{1}{2} - \frac{1.75}{t^2}$  is an increasing function, thus, the minimum value is this function in  $(2, +\infty]$  is  $\frac{1}{2} - \frac{1.75}{2^2} = 0.0625 > 0$ .

As a consequence  $\frac{1}{t}\Lambda(t)$  is an increasing monotone function for  $t \geq 0$ , thus,  $T_i \in IHRA$ ,  $i = 1, \dots, 5$ .

- **Duration of the bridge system**

$T$

- **Stochastic ageing character of  $T$**

According to Table 3.2, the *IHRA* property of the components of a system is preserved after the formation of a coherent system, like the bridge system. Thus,  $T \in IHRA$ .

- (b) *Estabeleça um limite inferior para a duração esperada da vida da estrutura, sabendo que a duração esperada comum das componentes é de aproximadamente 5.62 horas.* (2.0)

- **Lower bound for  $E(T)$**

We are dealing with a coherent system characterized as follows:

- the 5 components have durations  $T_i \stackrel{i.i.d.}{\sim} IHRA$ ,  $i = 1, \dots, 5$  and, thus, according to Proposition 3.36,

$$T_i \stackrel{i.i.d.}{\sim} NBUE, i = 1, \dots, 5;$$

- the expected value of the duration of each of the 5 components is equal to  $\mu^* = \mu_i = E(T_i) \simeq 5.62$ .

- the minimal path sets are

$$\mathcal{P}_1 = \{1, 24\}$$

$$\mathcal{P}_2 = \{2, 5\}$$

$$\mathcal{P}_3 = \{1, 3, 5\}$$

$$\mathcal{P}_4 = \{2, 3, 4\}$$

$$p = 5 \text{ minimal path sets.}$$

Now, we can apply Theorem 3.65, and conclude that

$$\begin{aligned} \mu &= E(T) \\ &\geq \max_{j=1, \dots, p} \left\{ \left( \sum_{i \in \mathcal{P}_j} \mu_i^{-1} \right)^{-1} \right\} \\ &\stackrel{\mu_i = \mu^*}{=} \max_{j=1, \dots, p} \left\{ \left( \frac{\#\mathcal{P}_j}{\mu^*} \right)^{-1} \right\} \\ &= \frac{\mu^*}{\min_{j=1, \dots, p} \{\#\mathcal{P}_j\}} \\ &= \frac{\mu^*}{2} \\ &= 2.81. \end{aligned}$$

4. *Um veículo de teste foi sujeito a uma rodagem de 25000Km, tendo-se registado os Kms percorridos entre falhas eléctricas graves sucessivas: 63, 51, 14166, 1825, 1288, 1314, 472, 3463, 486, 1017Km.*

- (a) *Averigue a adequação do modelo exponencial a este conjunto de dados considerando um nível de significância de 5%.* (2.0)

- **Life test**

Since the test was scheduled to end after exactly  $t_0 = 25000Km$  and the exercise mentions just one vehicle submitted to this life test, we are dealing with a

- Type I/item censored testing with replacement.

- **R.v.**

$T_{(i)}$  = time (in Km) of the  $i^{th}$  serious electrical failure of the military vehicle

$Z_i = T_{(i)} - T_{(i-1)}$  = run time (in Km) between the  $i^{th}$  and  $(i-1)^{th}$  serious electrical failure of the military vehicle

$$Z_i \stackrel{i.i.d.}{\sim} Z, i \in \mathbb{N}$$

- **Censored data**

$$n = 1$$

$r = 10$  electrical failures during the life test

$$(z_1, \dots, z_r) = 63, 51, 14166, 1825, 1288, 1314, 472, 3463, 486, 1017$$

$$(t_{(1)}, \dots, t_{(r)}) = (63, 114, 14820, 16105, 17393, 18707, 19179, 22642, 23128, 24145)$$

- **Cumulative total time in test**

According to Definition 5.17, the cumulative total time in test is given by:

$$\begin{aligned} \tilde{t} &= n \times t_0 \\ &= 1 \times 25000 \\ &= 25000Km \end{aligned}$$

- **Hypotheses**

$$H_0 : Z \sim \text{Exponential}(\lambda)$$

$$H_1 : Z \sim \text{Weibull}(\lambda^{-1}, \alpha), \alpha \neq 1$$

- **Significance level**

$$\alpha_0 = 5\%$$

- **Test statistic (Bartlett's test)**

$$\begin{aligned} B_r &\stackrel{(5.19)}{=} \frac{2r}{1 + \frac{r+1}{6r}} \left[ \ln \left( \frac{\sum_{i=1}^r Z_i}{r} \right) - \frac{1}{r} \sum_{i=1}^r \ln(Z_i) \right] \\ &\stackrel{a}{\sim}_{H_0} \chi_{(r-1)}^2 \end{aligned}$$

- **Rejection region of  $H_0$**

$$\begin{aligned} W &= \left( 0, F_{\chi_{(r-1)}^2}^{-1}(\alpha_0/2) \right) \cup \left( F_{\chi_{(r-1)}^2}^{-1}(1 - \alpha_0/2), +\infty \right) \\ &\stackrel{r=10, \alpha_0=0.05}{=} (0, 2.700) \cup (19.02, +\infty) \end{aligned}$$

- **Decision**

The observed value of the test statistic is

$$b_r = \frac{2r}{1 + \frac{r+1}{6r}} \left[ \ln \left( \frac{\sum_{i=1}^r z_i}{r} \right) - \frac{1}{r} \sum_{i=1}^r \ln(z_i) \right]$$

$$\begin{aligned}
&= \frac{2 \times 10}{1 + \frac{10+1}{6 \times 10}} \times \left[ \ln \left( \frac{24145}{10} \right) - \frac{1}{10} 69.902263 \right] \\
&= 18.575006 \\
&\notin (0, 2.700) \cup (19.02, +\infty),
\end{aligned}$$

therefore we should not reject  $H_0$  for any significance level  $\alpha \leq 5\%$ .

- (b) Após ter enunciado as hipóteses de trabalho que entender convenientes, obtenha uma estimativa centrada da função de fiabilidade aos 1200 Km e um intervalo de confiança a 95% para a kilometragem associada a 10% das falhas. (3.0)

- **Distribution assumption**

$T_i \stackrel{i.i.d.}{\sim} \text{Exponential}(\lambda)$ ,  $i = 1, \dots, 6$ .

This is fairly reasonable since we did not reject  $H_0$  in (a).

- **Unknown parameter**

$$R_T(t) = e^{-\lambda t}$$

- **Unbiased estimate of  $R_T(t)$**

According to Table 5.14, the UMVUE of  $R_T(t)$  is, for  $t = 1200 < \tilde{t} = 25000$  and  $r > 0$ , equal to

$$\begin{aligned}
\tilde{R}_T(t) &= (1 - \tilde{t}^{-1} \times t)^r \\
&= \left( 1 - \frac{1}{25000} \times 1200 \right)^{10} \\
&\simeq 0.611462.
\end{aligned}$$

- **Confidence interval for  $\lambda$**

According to Table 5.16 of the lecture notes,

$$\begin{aligned}
CI_{(1-\alpha) \times 100\%}(\lambda) &= [\lambda_L; \lambda_U] \\
&= \left[ \frac{F_{\chi^2_{(2r)}}^{-1}(\alpha/2)}{2 \times \tilde{t}}; \frac{F_{\chi^2_{(2r+2)}}^{-1}(1-\alpha/2)}{2 \times \tilde{t}} \right] \\
CI_{95\%}(\lambda) &\stackrel{a)}{=} \left[ \frac{F_{\chi^2_{(20)}}^{-1}(0.025)}{2 \times 1 \times 25000}; \frac{F_{\chi^2_{(22)}}^{-1}(0.975)}{2 \times 1 \times 25000} \right] \\
&= \left[ \frac{9.591}{50000}; \frac{36.78}{50000} \right] \\
&\simeq [0.000192; 0.000736].
\end{aligned}$$

- **Another unknown parameter**

$F_T^{-1}(0.1) = -\frac{1}{\lambda} \ln(1 - 0.1)$ , which is a decreasing function of  $\lambda > 0$ .

- **Confidence interval for  $F_T^{-1}(0.1)$**

$$\begin{aligned}
CI_{95\%}(F_T^{-1}(0.1)) &= \left[ \frac{1}{\lambda_U} \ln(1 - 0.1); \frac{1}{\lambda_L} \ln(1 - 0.1) \right] \\
&\simeq [143.237917; 549.291784].
\end{aligned}$$