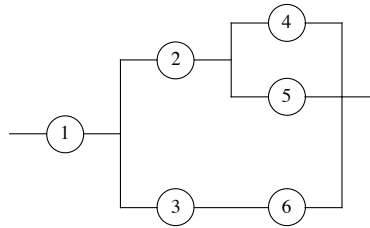


- Duration: **2 hours**
- Please justify your answers.
- This test has **two pages** and **seven questions**. The total of points is **20.0**.

1. A lifting station for wastewater containing sewage depends on six components set according to the following system block diagram:



(a) Identify the minimal path sets and minimal cut sets of this system, and provide an expression (do not simplify it!) for its structure function. (1.5)

• **Minimal path sets**

$$\mathcal{P}_1 = \{1, 2, 4\}, \quad \mathcal{P}_2 = \{1, 2, 5\}, \quad \mathcal{P}_3 = \{1, 3, 6\},$$

$p^* = 3$  minimal path sets

• **Minimal cut sets**

$$\mathcal{K}_1 = \{1\}, \quad \mathcal{K}_2 = \{2, 3\}, \quad \mathcal{K}_3 = \{2, 6\}, \quad \mathcal{K}_4 = \{4, 5, 3\} = \{3, 4, 5\}, \quad \mathcal{K}_5 = \{4, 5, 6\},$$

$q = 5$  minimal cut sets

• **Structure function**

$$\begin{aligned} \phi(\underline{X}) &\stackrel{Th.1.30}{=} 1 - \prod_{j=1}^{p^*} \left( 1 - \prod_{i \in \mathcal{P}_j} X_i \right) \\ &= 1 - (1 - X_1 X_2 X_4) \times (1 - X_1 X_2 X_5) \times (1 - X_1 X_3 X_6) \end{aligned}$$

**Obs.** — Equivalently,

$$\begin{aligned} \phi(\underline{X}) &\stackrel{Th.1.30}{=} \prod_{j=1}^q \left[ 1 - \prod_{i \in \mathcal{K}_j} (1 - X_i) \right] \\ &= [1 - (1 - X_1)] \times [1 - (1 - X_2)(1 - X_3)] \times [1 - (1 - X_2)(1 - X_6)] \\ &\quad \times [1 - (1 - X_3)(1 - X_4)(1 - X_5)] \times [1 - (1 - X_4)(1 - X_5)(1 - X_6)]. \end{aligned}$$

(b) Suppose now that the components operate independently and  $p_i = p = 0.99$ ,  $i = 1, \dots, 6$ . Provide two non trivial lower bounds for the reliability of the system. Which bound is stricter? (1.5)

• **Reliability of the components**

$$p_i = p = 0.99, \quad i = 1, \dots, 6$$

• **First lower bound for  $r(p)$**

The components form a coherent system and operate independently, therefore

$$\begin{aligned} \underline{r(p)} &\stackrel{Th.1.68}{\geq} \prod_{j=1}^q \left[ 1 - \prod_{i \in \mathcal{K}_j} (1 - p) \right] \stackrel{p_i=p}{=} \prod_{j=1}^q [1 - (1 - p)^{\#\mathcal{K}_j}] \\ &= [1 - (1 - p)] \times [1 - (1 - p)^2]^2 \times [1 - (1 - p)^3]^2 \\ &\stackrel{p=0.99}{=} 0.989800. \end{aligned}$$

- **Second lower bound for  $r(p)$**

Since the components form a coherent system and operate in an independent fashion — hence, in a positively associated manner —, we can also apply Theorem 1.70 (min-max bounds!).

$$r(\underline{p}) \stackrel{(1.42)}{\geq} \max_{j=1, \dots, p^*} \prod_{i \in \mathcal{D}_j} p_i \stackrel{p_i = p}{=} \max_{j=1, \dots, p^*} p^{\#\mathcal{D}_j} = p^{\min_{j=1, \dots, p^*} \#\mathcal{D}_j} = p^3 = 0.970299.$$

- **Which bound is stricter ?**

Since  $0.989800 > 0.970299$  the lower bound given by Theorem 1.68 is stricter than the one obtain by invoking Theorem 1.70.

2. A leaf spring for a truck is assumed to have a time to failure ( $X$ , in years) with hazard rate function equal to  $\lambda(t) = \left(\frac{t}{4}\right)^3, t \geq 0$ .

(a) What is the probability that this leaf spring fails after age  $E(X) = 4 \times \Gamma(1/4 + 1)$  ?

(1.5)

**Obs.:** It might be useful to know that  $\Gamma(1/4) \simeq 3.625610$ .

- **R.v.**

$X$  = time to failure of a leaf spring for a truck

- **Hazard rate function**

$$\lambda(t) = \left(\frac{t}{4}\right)^3, t \geq 0$$

- **Survival function**

Using Prop. 3.3, we get

$$\begin{aligned} R(t) &= \exp\left[-\int_0^t \lambda(u) du\right] \\ &= \exp\left[-\int_0^t \left(\frac{u}{4}\right)^3 du\right] \\ &= \exp\left[-\left(\frac{u}{4}\right)^4 \Big|_0^t\right] \\ &= \exp\left[-\left(\frac{t}{4}\right)^4\right], t \geq 0. \end{aligned}$$

- **Requested probability**

Since  $E(X) = 4 \times \Gamma(1/4 + 1) = 4 \times \frac{1}{4} \Gamma(1/4) \simeq 3.625610$ , we get

$$\begin{aligned} R[E(X)] &= \exp\left\{-\left[\frac{E(X)}{4}\right]^4\right\} \\ &\simeq \exp\left(-\frac{3.625610^4}{256}\right) \\ &\simeq 0.509172. \end{aligned}$$

(b) Assume that:  $T_i$  represents the time to failure of the leaf spring  $i$  ( $i = 1, \dots, 4$ ) and  $T_i \sim i.i.d. X$ ; 3 out of 4 leaf springs are crucial from a safety standpoint of the truck. (1.5)

Derive the reliability function of the associated time to failure ?

- **Individual times to failure, common reliability function**

$T_i$  = time to failure of leaf spring  $i, i = 1, \dots, 4$

$$T_i \stackrel{i.i.d.}{\sim} X, i = 1, \dots, 4$$

$$R_i(t) = R(t) = \exp\left[-\left(\frac{t}{4}\right)^4\right], t \geq 0$$

- **Duration of the system**

We are dealing with a 3-out-of-4 system, thus

$$T = T_{(n-k+1)} = T_{(4-3+1)} = T_{(2)}.$$

• **Reliability function of  $T$**

$$\begin{aligned}
 R_T(t) &\stackrel{(2.8)}{=} F_{binomial(4,1-R(t))}(4-3) \\
 &= \sum_{j=0}^1 \binom{4}{j} [1-R(t)]^j [R(t)]^{4-j} \\
 &= [R(t)]^4 + 4[1-R(t)][R(t)]^3 \\
 &= 4[R(t)]^3 - 3[R(t)]^4 \\
 &= 4e^{-\frac{3t^4}{256}} - 3e^{-\frac{t^4}{64}}, \quad t \geq 0.
 \end{aligned}$$

(c) What can be said about the stochastic ageing character of this system with four leaf springs? (0.5)

• **Devising the stochastic ageing character of  $T$**

Since  $\lambda(t) = \left(\frac{t}{4}\right)^3$ ,  $t \geq 0$ , is an increasing function in  $t$ , we can conclude that  $T_i \stackrel{i.i.d.}{\sim} IHR$ ,  $i = 1, \dots, 4$ . By applying Prop. 3.25, we can add that any order statistic is also IHR, namely

$$T = T_{(2)} \in IHR.$$

(d) Now, suppose the four leaf springs operate in a positively associated manner. (2.0)

Obtain an appropriate lower bound for the expected time to failure of this *new* system.

• **Important**

We are dealing with positively associated r.v. therefore we can resort to Theorem 2.22 to provide bounds for  $R_T$ .

• **Lower bound for  $R_T(t)$**

Note that the minimal path sets associated with a 3-out-of-4 system are

$$\mathcal{P}_1 = \{1, 2, 3\}, \quad \mathcal{P}_2 = \{1, 2, 4\}, \quad \mathcal{P}_3 = \{1, 3, 4\}, \quad \mathcal{P}_4 = \{2, 3, 4\}, \quad p^* = 4 \text{ minimal path sets.}$$

Consequently, by invoking Theorem 2.22, we get

$$R_T(t) \geq \max_{j=1, \dots, p^*} \left[ \prod_{i \in \mathcal{P}_j} R_i(t) \right] \stackrel{R_i(t) = R(t)}{=} \max_{j=1, \dots, p^*} [R(t)]^{\#\mathcal{P}_j} = [R(t)]^{\min_{j=1, \dots, p^*} \#\mathcal{P}_j} \stackrel{\#\mathcal{P}_j = 3, \forall j}{=} [R(t)]^3.$$

• **Lower bound for  $\mu$**

$$\begin{aligned}
 E(T) &\stackrel{(2.10)}{=} \int_0^{+\infty} R_T(t) dt \\
 &\geq \int_0^{+\infty} [R(t)]^3 dt \\
 &\stackrel{(b)}{=} \int_0^{+\infty} \exp \left[ -3 \times \left( \frac{t}{4} \right)^4 \right] dt \\
 &\stackrel{(b)}{=} \int_0^{+\infty} R_{Weibull(\frac{4}{3^{1/4}}, 4)}(t) dt \\
 &= \frac{4}{3^{1/4}} \times \Gamma(1/4 + 1) \\
 &= \frac{1}{3^{1/4}} \times \Gamma(1/4) \\
 &\approx 2.754868.
 \end{aligned}$$

3. Twenty-four vehicles have completed a 74 000 kilometer scheduled run at an automobile company's proving grounds. During the test eight radiator hoses failed and were replaced at kilometers: 2 760, 3 700, 7 100, 17 220, 29 500, 48 400, 52 600, 65 000. (1.5)

Calculate the ML estimate of the expected number of replacements of the original radiator hoses during the 24 000 kilometer warranty period supposing that: two million vehicles have been sold; proving ground kilometers are assumed to be equivalent to customer kilometers; the times to replacement are independent and exponentially distributed.

- **Failure times**

$T_i$  = failure time of a radiator hose  $i$

$T_i \stackrel{i.i.d.}{\sim} \text{exponential}(\lambda)$ ,  $i = 1, \dots, n$  ( $n = 20$ )

$\lambda > 0$  (UNKNOWN)

- **Censored data**

Since the test lasted for  $t_0 = 74\,000$  hours and none of the  $r = 8$  failed radiator hoses was replaced, we are dealing with a Type I/item censored testing with replacement.

- **Total time on test**

According to Definition 5.17, the cumulative total time in test is in this particular case:

$$\begin{aligned}\tilde{t} &= n \times t_0 \\ &= 24 \times 74\,000 \\ &= 1\,776\,000\end{aligned}$$

- **ML estimate of  $\lambda$**

According to Table 5.11, it is equal to

$$\begin{aligned}\hat{\lambda} &= \frac{r}{\tilde{t}} \\ &= \frac{8}{1\,776\,000}.\end{aligned}$$

- **Another unknown parameter**

If two million vehicles are sold, then the r.v.  $Y$ , representing number of replacements of the original radiator hoses during the 24 000 kilometer warranty period, has a binomial distribution with parameters  $m = 2\,000\,000$  and  $p = P(T \leq 24\,000) = 1 - e^{-24\,000 \times \lambda}$ .

Its expected value is equal to

$$h(\lambda) = 2\,000\,000 \times \left(1 - e^{-24\,000 \times \lambda}\right).$$

- **Requested ML estimate**

By invoking the invariance property of the ML estimators, we can add that

$$\begin{aligned}\widehat{h(\lambda)} &= h(\hat{\lambda}) \\ &= 2\,000\,000 \times \left(1 - e^{-24\,000 \times \hat{\lambda}}\right) \\ &= 2\,000\,000 \times \left(1 - e^{-24\,000 \times \frac{8}{1\,776\,000}}\right) \\ &\simeq 204\,938.878.\end{aligned}$$

4. The target fraction of live births from c-sections is  $p_0 = 0.15$ .

(a) A sample of 125 live births led to 25 c-sections performed in the sample. When plotted on a  $p$ -chart with 3-sigma control limits, what does the observed value of the control statistic suggest? (0.5)

- **Answer**

The observed value of the control statistic is equal to  $t = \frac{25}{125} = 0.2$ . Since it is above the center line  $p_0 = 0.15$ , we only need to calculate the

$$UCL = p_0 + 3\sqrt{\frac{p_0(1-p_0)}{n}} = 0.15 + 3\sqrt{\frac{0.15(1-0.15)}{125}} \simeq 0.245812,$$

and conclude that  $t < UCL$ , thus the observed value of the control statistic suggests that the fraction of c-sections is in-control.

(b) Obtain an approximate value of the in-control ARL of the  $np$ -chart used to control the fraction of (1.5)

c-sections, with  $n = 20$ ,  $p_0 = 0.15$ , and 3-sigma control limits.

- **Control statistic of the  $np$ -chart and its distribution**

$Y_N$  = number of nonconforming items in the  $N^{th}$  batch,  $N \in \mathbb{N}$

$Y_N \sim \text{binomial}(n, p)$

- **3-sigma control limits**

$$\begin{aligned} LCL &= \left\lceil \max\{0, np_0 - 3 \times \sqrt{np_0(1-p_0)}\} \right\rceil = \left\lceil \max\{0, 20 \times 0.15 - 3 \times \sqrt{20 \times 0.15 \times (1-0.15)}\} \right\rceil \\ &= \left\lceil \max\{0, 3 - 3\sqrt{2.55}\} \right\rceil = \lceil \max\{0, -1.791\} \rceil = 0 \end{aligned}$$

$$\begin{aligned} UCL &= \left\lceil np_0 + 3 \times \sqrt{np_0(1-p_0)} \right\rceil = \left\lceil 20 \times 0.15 + 3 \times \sqrt{20 \times 0.15 \times (1-0.15)} \right\rceil \\ &= \left\lceil 3 + 3\sqrt{2.55} \right\rceil = \lceil 7.791 \rceil = 7. \end{aligned}$$

- **Probability of triggering a signal**

$$\begin{aligned} \xi(\theta) &= 1 \times P(Y_N \notin [LCL, UCL] \mid p = p_0 + \theta) \\ &= 1 - [F_{\text{binomial}(n, p_0 + \theta)}(UCL) - F_{\text{binomial}(p_0 + \theta)}(LCL - 1)]. \end{aligned}$$

- **Requested in-control ARL**

Since  $RL(0) \sim \text{geometric}(\xi(0))$ ,

$$\begin{aligned} ARL(0) &= \frac{1}{\xi(0)} = \frac{1}{1 - [F_{\text{binomial}(20, 0.15+0)}(7) - F_{\text{binomial}(20, 0.15+0)}(0-1)]} \\ &\stackrel{\text{tables}}{=} \frac{1}{1 - 0.9941 + 0} \\ &\approx 169.492. \end{aligned}$$

- **[Obs.:** If we use a calculator instead of the tables then  $ARL(0) \approx 168.886$ .]

5. An engineer is monitoring the proportion  $p$  of incompletely filled low voltage liquid crystal display units in a high-yield process. The associated control statistic  $X$  is the cumulative count of conforming display units between two nonconforming ones. The p.f. and c.d.f. of  $X$  is given by  $P_p(X = x) = (1-p)^x p$ ,  $x \in \mathbb{N}_0$ , and  $F_p(x) = 1 - (1-p)^{1+x}$ ,  $x \in \mathbb{N}_0$ , where the target value of  $p$  is known and denoted by  $p_0 \in (0, 1)$  and the true value of  $p$  is equal to  $\rho \times p_0$ , with  $0 < \rho < 1/p_0$ .

- (a) The engineer is planning to use a chart with conventional  $k$ -sigma control limits ( $k \in \mathbb{R}^+$ ): (1.5)
- $$LCL = (1-p_0)/p_0 - k \sqrt{1-p_0}/p_0 \text{ and } UCL = (1-p_0)/p_0 + k \sqrt{1-p_0}/p_0.$$

For which values of  $k$  is the LCL positive?

Elaborate on the importance of a positive LCL in this particular context.

- **Control statistic**

$X$  = number of nonconforming items between two consecutive conforming items

$X \sim \text{geometric}^*(p)$

- **P.f., c.d.f., expected value and variance of the control statistic**

$$P_p(X = x) = (1-p)^x p, x \in \mathbb{N}_0$$

$$F_p(x) = 1 - (1-p)^{1+x}, x \in \mathbb{N}_0$$

$$E_p(X) = \frac{1-p}{p}$$

$$V_p(X) = \frac{1-p}{p^2}$$

- **[On the control limits**

They are equal to:

$$E_{p_0}(X) \pm k \sqrt{V_{p_0}(X)} = \frac{1-p_0}{p_0} \pm k \sqrt{\frac{1-p_0}{p_0^2}}, \quad k > 0.]$$

- **Requested values of  $k$**

$$k \in \mathbb{R}^+ : LCL > 0 \Leftrightarrow (1-p_0)/p_0 - k \sqrt{(1-p_0)/p_0^2} > 0 \Leftrightarrow k < \sqrt{1-p_0}.$$

- **Importance of a positive LCL**

It is essential that the chart has a positive LCL so the chart is able to detect increases in  $p$  (i.e., to detect a quality deterioration) in a fairly quick fashion.

If  $LCL \neq 0$ , we are bound to deal with an upper one-sided chart, whose out-of-control ARL in the presence of some increases in  $p$  is surely (and unreasonably) larger than the in-control ARL.

(b) A statistician anticipated both downward and upward shifts and decided to adopt an alternative chart with control limits  $LCL^* = 4$  and  $UCL^* = 7428$ . Moreover, it triggers a signal with probability: (2.0)

- one if the control statistic  $X$  is below  $LCL^*$  or above  $UCL^*$ ;
- $\gamma_{LCL^*} = 0.415872$  (resp.  $\gamma_{UCL^*} = 0.349557$ ) if the control statistic is equal to  $LCL^*$  (resp.  $UCL^*$ ).

The in-control ARL of this new chart is equal to  $1/\alpha = 200$ .

Verify that, when  $p$  shifts from its target value  $p_0 = 0.001$  to  $p = 1.1 \times p_0$ , the out-of-control ARL is approximately equal to 194.950. Comment on this ARL value.

- **Probability of a signal**

Judging by the description above, when  $p = \rho \times p_0$  ( $\rho \in (0, 1/p_0)$ ), this alternative chart triggers a signal with probability

$$\begin{aligned} \xi^*(\rho) &= 1 \times \{1 - \{F_{\rho \times p_0}(UCL^*) - F_{\rho \times p_0}[(LCL^*)^-]\}\} \\ &\quad + \gamma_{LCL^*} \times P_{\rho \times p_0}(X = LCL^*) \\ &\quad + \gamma_{UCL^*} \times P_{\rho \times p_0}(X = UCL^*) \\ &= [1 - (1 - \rho \times 0.001)^{1+(4-1)} + (1 - \rho \times 0.001)^{1+7428}] \\ &\quad + 0.415872 \times (1 - \rho \times 0.001)^4 \rho \times 0.001 \\ &\quad + 0.349557 \times (1 - \rho \times 0.001)^{7428} \rho \times 0.001. \end{aligned}$$

Thus, the probability of a valid signal, when  $\rho = 1.1$ , is given by

$$\begin{aligned} \xi^*(1.1) &= [1 + (1 - 1.1 \times 0.001)^{1+7428} - (1 - 1.1 \times 0.001)^{1+4}] \\ &\quad + 0.415872 \times (1 - 1.1 \times 0.001)^4 1.1 \times 0.001 \\ &\quad + 0.349557 \times (1 - 1.1 \times 0.001)^{7428} 1.1 \times 0.001 \\ &\approx 0.005130. \end{aligned}$$

- **ARL function and requested ARL value**

Since we are still dealing with a Shewhart chart with independent control statistics, we have

$$\begin{aligned} ARL^*(\rho) &= \frac{1}{\xi^*(\rho)} \\ ARL^*(1.1) &= \frac{1}{0.005130} \\ &\approx 194.950. \end{aligned}$$

- **Comment**

This chart is able to signal an increase in  $p$  sooner (in average) than to trigger a false alarm —  $ARL^*(1) > ARL^*(1.1)$  — a very desirable property.

6. The high-voltage output of a certain power supply used in a copy machine is assumed to have a normal distribution with nominal mean and standard deviation equal to  $\mu_0 = 350$  and  $\sigma_0 = 2.0$  (V dc at 20 milliamps). Samples of  $n = 9$  power supply units have been inspected every half-hour. The process mean and standard deviation have increased and the magnitudes of the associated shifts are  $\delta = \sqrt{n}(\mu - \mu_0)/\sigma_0 = 0.25$  and  $\theta = \sigma/\sigma_0 = \sqrt{23.574603/21.95}$ , respectively.

Obtain and interpret the first quartile of the out-of-control RL of a  $\bar{X}$ -chart with 3-sigma limits.

- **Quality characteristic**

$X$  = high-voltage output of a certain power supply used in a copy machine

$$X \sim \text{normal}(\mu, \sigma^2)$$

- **Control statistic of the standard  $\bar{X}$ -chart and its distribution**

$\bar{X}_N$  = mean of the  $N^{\text{th}}$  random sample of size  $n$

$\bar{X}_N \sim \text{normal}\left(\mu = \mu_0 + \delta \times \frac{\sigma_0}{\sqrt{n}}, \frac{\sigma^2}{n} = \frac{(\theta\sigma_0)^2}{n}\right)$ , where  $\delta \in \mathbb{R}$  (resp.  $\theta \geq 1$ ) represents the magnitude of a shift in  $\mu$  (resp. an upward shift in  $\sigma$ )

- **Control limits**

$$LCL_\mu = \mu_0 - \gamma_\mu \times \frac{\sigma_0}{\sqrt{n}}$$

$$UCL_\mu = \mu_0 + \gamma_\mu \times \frac{\sigma_0}{\sqrt{n}},$$

where  $\gamma_\mu = 3$ ,  $\mu_0 = 350$  and  $\sigma_0 = 2.0$ .

- **Shifts in the process mean and standard deviation**

$$\delta = \sqrt{n}(\mu - \mu_0) / \sigma_0 = 0.25$$

$$\theta = \frac{\sigma}{\sigma_0} = \sqrt{\frac{23.574603}{21.95}} \simeq 1.036346$$

- **Probability of a signal**

$$\begin{aligned} \xi_\mu(\delta, \theta) &= P(\bar{X}_N \notin [LCL_\mu, UCL_\mu] \mid \delta, \theta) \\ &= \dots \\ &= 1 - \left[ \Phi\left(\frac{\gamma_\mu - \delta}{\theta}\right) - \Phi\left(\frac{-\gamma_\mu - \delta}{\theta}\right) \right] \\ &= 1 - \left[ \Phi\left(\frac{3 - 0.25}{1.036346}\right) - \Phi\left(\frac{-3 - 0.25}{1.036346}\right) \right] \\ &\simeq 1 - [\Phi(2.65) - \Phi(-3.14)] \\ &\stackrel{\text{tables}}{=} 1 - [0.9960 - (1 - 0.999155)] \\ &= 0.004845 \end{aligned}$$

- **Requested 25% percentage point of the out-of-control  $RL_\mu$**

Given that  $RL_\mu(\delta, \theta) \sim \text{geometric}(\xi_\mu(\delta, \theta))$ , we have

$$\begin{aligned} F_{RL_\mu(\delta, \theta)}^{-1}(p) &\stackrel{\text{Table 9.1}}{=} \inf\{m \in \mathbb{N} : F_{RL_\mu(\delta, \theta)}(m) \geq p\} \\ &= \left\lceil \frac{\ln(1-p)}{\ln[1-\xi_\mu(\delta, \theta)]} \right\rceil \\ &= \left\lceil \frac{\ln(1-0.25)}{\ln(1-0.004845)} \right\rceil \\ &= [59.233] \\ &= 60. \end{aligned}$$

- **Interpretation of the  $F_{RL_\mu(\delta, \theta)}^{-1}(0.25)$**

When there is a shift in the location and spread of this quality characteristic with magnitude  $(\delta, \theta) = (0.25, \sqrt{23.574603/21.95})$ , the probability that the  $\bar{X}$ -chart triggers a valid signal within the first 60 samples is of at least 25%.

7. The drained weight after filling of contents of a can of tomatoes is required to be at most 22.8 oz.

(a) Consider a sampling plan by variables with UNKNOWN STANDARD DEVIATION,  $(n_s, k_s) = (2.0, (59, 1.937713))$ , and risk points  $(p_1, 1 - \alpha) = (1\%, 0.95)$  and  $(p_2, \beta) = (5\%, 0.1)$ .

Confirm that this plan is indeed related to these risk points and compare  $(n_s, k_s)$  to  $(n_\sigma, k_\sigma) = (19, 1.943305)$ .

• **Single sampling plan by variables with UNKNOWN STANDARD DEVIATION**

$n_s$  (sample size)

$k_s$  (acceptance constant)

• **Producer's and consumer's risk points**

$(p_1, 1 - \alpha) = (1\%, 0.95)$

$(p_2, \beta) = (5\%, 0.1)$

• **Requested verification**

If we consider  $n_s = 59$  and  $k_s = 1.937713$  then

$$\begin{aligned}
 P_a(p_1) &\stackrel{(13.39)}{\approx} \Phi(\theta_{p_1}) \\
 &\stackrel{(13.41)}{\approx} \Phi \left[ \frac{\Phi^{-1}(1 - p_1) - k_s \sqrt{\frac{3n_s - 4}{3n_s - 3}}}{\sqrt{1 + \frac{3n_s k_s^2}{6n_s - 8}}} \right] \\
 &= \Phi \left[ \frac{2.3263 - 1.937713 \sqrt{\frac{3 \times 59 - 4}{3 \times 59 - 3}}}{\sqrt{1 + \frac{3 \times 59 \times 1.937713^2}{6 \times 59 - 8}}} \right] \\
 &\approx \Phi(1.77) \\
 &\stackrel{table}{=} 0.9616 \\
 &\geq 1 - \alpha = 0.95 \\
 P_a(p_2) &\approx \Phi(\theta_{p_2}) = \Phi \left[ \frac{1.6449 - 1.937713 \sqrt{\frac{3 \times 59 - 4}{3 \times 59 - 3}}}{\sqrt{1 + \frac{3 \times 59 \times 1.937713^2}{6 \times 59 - 8}}} \right] \\
 &\approx \Phi(-1.29) \\
 &\stackrel{table}{=} 1 - 0.9015 \\
 &= 0.0985 \\
 &\leq \beta = 0.1.
 \end{aligned}$$

Hence, the sampling plan complies with the two given risk points.

• **Comment**

Admitting that the standard deviation is unknown is more realistic:

- it does not change the acceptance constant significantly (in this exercise  $k_s \approx k_\sigma$  down to the first decimal place);
- but it requires the collection of a much larger sample (in this case  $n_s = 3.1 \times n_\sigma$ ).

(b) Suppose a sample of size  $n_s$  was taken from a lot, and  $\bar{x} = 22.876942$ ,  $s = 1.116276$ . (0.5)

Should the lot be accepted or rejected?

• **Checking whether or not the lot should be accepted**

The lot should be accepted iff

$$Q = \frac{U - \bar{x}}{s} \geq k_s,$$

where  $Q$  is the quality index,  $U$  is the upper specification limit,  $\bar{x}$  and  $s$  represent the mean of a sample with size  $n_s$ , and  $k_s$  the acceptance constant. For this sample, we have

$$\begin{aligned}
 Q &= \frac{22.8 - 22.876942}{1.116276} \\
 &= -0.068927 \\
 &\not\geq 1.937713,
 \end{aligned}$$

therefore we should reject the lot.